



MAX PLANCK INSTITUTE  
FOR DYNAMICS OF COMPLEX  
TECHNICAL SYSTEMS  
MAGDEBURG



COMPUTATIONAL METHODS IN  
SYSTEMS AND CONTROL THEORY

# Feedback Stabilization of Unsteady Flow Problems

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**TU Kaiserslautern**

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## Optimal Control

is used for the **optimization** of **dynamical processes**,  
described by ordinary or partial differential equations.

This is achieved by minimizing a **cost functional**  
(penalizing, e.g. energy consumption, deviation from reference trajectory),  
such that a prescribed target  
is reached **in given** or **minimal time**  
whilst complying with given control and state constraints.



Let  $(x_*, u_*)$  solve  $\min_{u \in \mathcal{U}_{ad}} J(x, u)$  **s.t.**  $\dot{x}(t) = f(x(t), u(t))$ .



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### Fundamental observation

Optimized trajectory  $x_*(t; u_*)$  and precomputed optimal control  $u_*(t)$  will not be attainable in practice due to

- modeling errors and/or unmodeled dynamics,
- model uncertainties,
- external perturbations,
- measurement errors.





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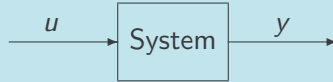
**Consequence:** need **feedback control**

$$u(t) = u_*(t) + U(t, x(t) - x_*(t))$$

in order to attenuate perturbations/errors!

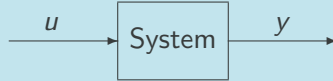


## Open-loop control/optimization

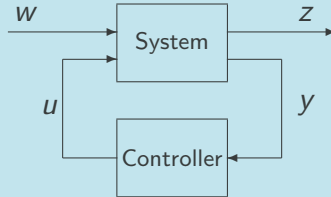




## Open-loop control/optimization



## Closed-loop/feedback control/optimization





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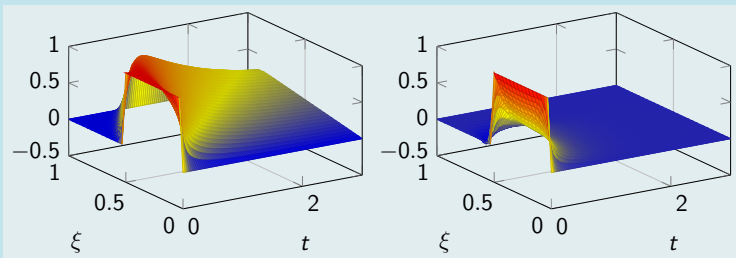




## Example: Optimal control of a simple transport model

Burgers' equation:

$$\begin{aligned}\partial_t x(t, \xi) &= \nu \partial_{\xi\xi} x(t, \xi) - x(t, \xi) \partial_{\xi} x(t, \xi) + B(\xi)u(t), \\ x(t, 0) &= x(t, 1) = 0, \quad x(0, \xi) = x_0(\xi), \quad \xi \in (0, 1), \\ y(t, \xi) &= C x(t, \xi).\end{aligned}$$



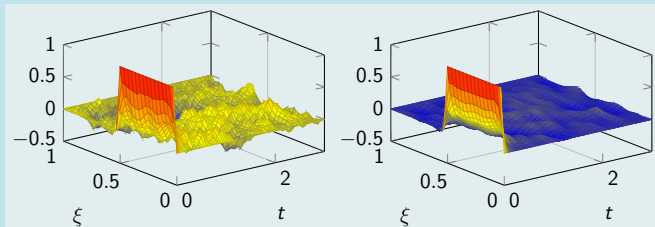


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Nonlinear control (here: MPC-LQG):

**Reduction of tracking error  $\int_0^T \|x(t) - x_*(t)\|_2^2 dt$  by factor  $> 10$ .**

[BENNER/GRNER, PAMM 2006]; [BENNER/GRNER/SAAK, Springer LNCSE 2006].



### The Linear-Quadratic Regulator (LQR) Problem

Minimize  $\mathcal{J}(u) = \frac{1}{2} \int_0^{\infty} (y^T Q y + u^T R u) dt$  for  $u \in \mathcal{L}_2(0, \infty; \mathbb{R}^m)$ ,

subject to

$$\dot{x}(t) = Ax(t) + Bu(t), \quad x(0) = x_0,$$

$$y(t) = Cx(t),$$

where  $A \in \mathbb{R}^{n \times n}$ ,  $B \in \mathbb{R}^{n \times m}$ ,  $C \in \mathbb{R}^{p \times n}$ .



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Solution of finite-dimensional LQR problem: **feedback control**

$$u_*(t) = -B^T X_* x(t) =: -K_* x(t),$$

where  $X_* = X_*^T \geq 0$  is the unique **stabilizing**<sup>1</sup> solution of the **algebraic Riccati equation (ARE)**

$$0 = \mathcal{R}(X) := C^T Q C + A^T X + X A - X B R^{-1} B^T X.$$

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<sup>1</sup> $X$  is stabilizing  $\Leftrightarrow \Lambda(A - B B^T X) \subset \mathbb{C}^-$ .





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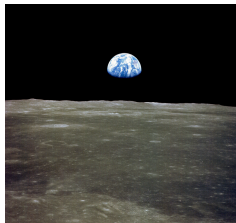
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**Linear-quadratic Gaussian (LQG) controller:** in LQR feedback law, replace state  $x$  by **state estimation**  $\hat{x}$  obtained by **Kalman-Bucy filter**.

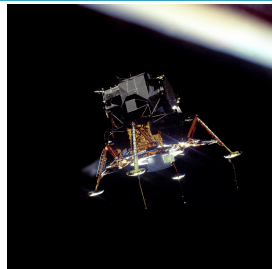
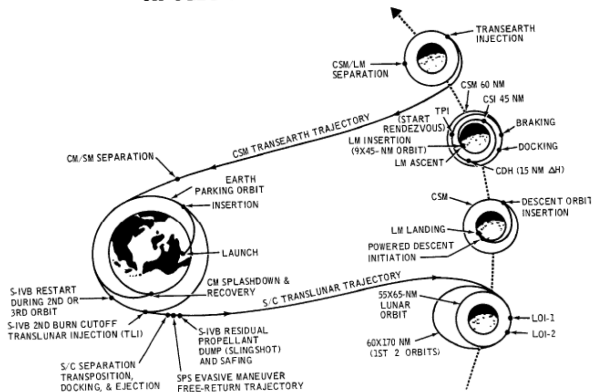


CSC

# Motivation — LQG Control: a Success Story! —



## APOLLO 11 FLIGHT PROFILE



By courtesy of:

middle  
left/right, top  
left/right, bottom

Apollo 11 Mission Operations report, [http://history.nasa.gov/alsj/a11/A11\\_MissionOpReport.pdf](http://history.nasa.gov/alsj/a11/A11_MissionOpReport.pdf)  
[http://de.wikipedia.org/wiki/Apollo\\_11](http://de.wikipedia.org/wiki/Apollo_11),  
NASA photo IDs AS11-44-6552, S69-42583.



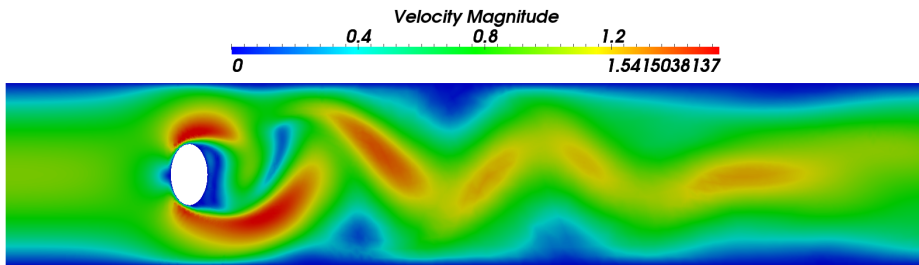
- **Physical transport** is one of the most fundamental dynamical processes in nature.
  - **Prediction** and **manipulation** of transport processes are important research topics, e.g., to
    - avoid stall — for stable and safe flight;
    - save energy (or increase attainable speed) by minimizing drag coefficient;
    - use fluid flow for optimal transport (e.g., in blood veins).
  - **Open-loop** controllers are widely used in various engineering fields.  
→ **Not robust** regarding perturbation
  - Dynamical systems are often influenced via so called **distributed control**.  
→ **Unfeasible** in many real-world areas
- ⇒ **Boundary feedback stabilization (closed-loop)**  
should be used to increase robustness and feasibility.



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2. Feedback Stabilization for Index-2 DAE Systems
3. Accelerated Solution of Riccati Equations
4. Conclusions



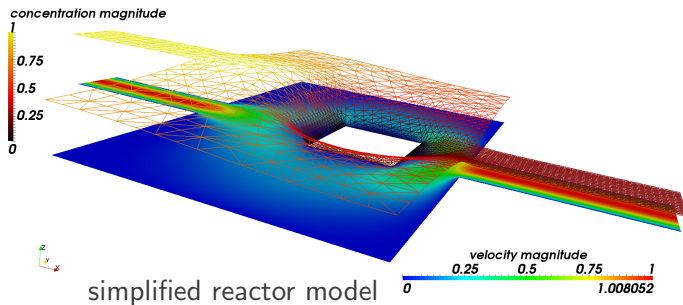
- Consider 2D flow problems described by **incompressible Navier–Stokes equations**.
- Riccati feedback approach requires the solution of an **algebraic Riccati equation**.
- Conservation of mass introduces a **divergence-freeness** condition  $\rightsquigarrow$  problems with mathematical basis of control design schemes.



Kármán vortex street



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- **Coupling** flow problems with a **scalar reaction-advection-diffusion equation**.





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**Develop techniques to deal with complex-shifted multi-field flow systems.**

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- include feedback into forward simulation within NAVIER
  - ⇒ closed-loop forward flow simulation

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### Navier–Stokes Equations

$$\frac{\partial \vec{v}}{\partial t} - \frac{1}{\text{Re}} \Delta \vec{v} + (\vec{v} \cdot \nabla) \vec{v} + \nabla p = \vec{f}$$
$$\text{div } \vec{v} = 0$$

- defined for time  $t \in (0, \infty)$  and space  $\vec{x} \in \Omega \subset \mathbb{R}^2$  bounded with  $\Gamma = \partial\Omega$
- + boundary and initial conditions
- initial boundary value problem with additional algebraic constraints





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$$A, M \in \mathbb{R}^{n \times n}, \hat{G} \in \mathbb{R}^{n \times n_p}$$

$$B \in \mathbb{R}^{n \times n_r}, C \in \mathbb{R}^{n_a \times n}$$

$$\mathbf{u}(t) \in \mathbb{R}^{n_r}, \mathbf{y}(t) \in \mathbb{R}^{n_a}$$

$$\text{rank}(\hat{G}) = n_p$$

## Linearize + Discretize $\rightarrow$ Index-2 DAE

$$M \frac{d}{dt} \mathbf{v}(t) = A \mathbf{v}(t) + \hat{G} \mathbf{p}(t) + B \mathbf{u}(t)$$

$$0 = \hat{G}^T \mathbf{v}(t)$$

$$\mathbf{y}(t) = C \mathbf{v}(t)$$

$$M = M^T \succ 0$$

$$\mathbf{v}(t) \in \mathbb{R}^n, \mathbf{p}(t) \in \mathbb{R}^{n_p}$$

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Show that projection in [HEI/SOR/SUN '08] is discretized version of Leray projector in [RAY '06].

$$M \Pi^T = \Pi M \quad \wedge \quad \Pi^T \mathbf{v} = \mathbf{v}_{\text{div},0}$$

[**Bänsch**/B./**SAAK**/**Stoll**/WEICHELT '13,'15]



### Navier–Stokes Equations

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### Concentration Equation

$$\frac{\partial c(\vec{v})}{\partial t} - \frac{1}{\text{Re Sc}} \Delta c(\vec{v}) + (\vec{v} \cdot \nabla) c(\vec{v}) = 0$$

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### Concentration Equation

$$\frac{\partial c(\vec{v})}{\partial t} - \frac{1}{\text{Re Sc}} \Delta c(\vec{v}) + (\vec{v} \cdot \nabla) c(\vec{v}) = 0$$

$$A, M \in \mathbb{R}^{n \times n}, \hat{G} \in \mathbb{R}^{n \times n_p}$$

$$B \in \mathbb{R}^{n \times n_r}, C \in \mathbb{R}^{n_a \times n}$$

$$\mathbf{u}(t) \in \mathbb{R}^{n_r}, \mathbf{y}(t) \in \mathbb{R}^{n_a}$$

$$\text{rank}(\hat{G}) = n_p$$

### Linearize + Discretize → Index-2 DAE

$$M \frac{d}{dt} \mathbf{x}(t) = A \mathbf{x}(t) + \hat{G} \mathbf{p}(t) + B \mathbf{u}(t)$$

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$$M = M^T \succ 0$$

$$\mathbf{x}(t) = \begin{bmatrix} \mathbf{v}(t) \\ \mathbf{c}(t) \end{bmatrix} \in \mathbb{R}^n$$

$$n = n_v + n_c, N = n + n_p$$

Show that projection in [HEI/SOR/SUN '08] is discretized version of Leray projector in [RAY '06].

$$M \Pi^T = \Pi M \quad \wedge \quad \Pi^T \mathbf{v} = \mathbf{v}_{\text{div},0}$$

[Bänsch/B./SAAK/Stoll/WEICHELT '13,'15]



### Navier–Stokes Equations

$$\frac{\partial \vec{v}}{\partial t} - \frac{1}{\text{Re}} \Delta \vec{v} + (\vec{v} \cdot \nabla) \vec{v} + \nabla p = \vec{f}$$

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[BÄNSCH/B./SAAK/STOLL/WEICHELT '13,'15]

Extension to coupled flow case, i.e.,

$$\hat{\Pi} := \begin{bmatrix} \Pi & 0 \\ 0 & I \end{bmatrix} \wedge \begin{bmatrix} \Pi^T & 0 \\ 0 & I \end{bmatrix} \begin{bmatrix} \mathbf{v} \\ \mathbf{c} \end{bmatrix} = \begin{bmatrix} \mathbf{v}_{\text{div},0} \\ \mathbf{c} \end{bmatrix}.$$

[BÄNSCH/B./SAAK/WEICHELT '14]



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[BÄNSCH/B./SAAK/WEICHELT '14]



## Helmholtz Decomposition

[GIRAULT/RAVIART '86]

■ Splitting:

$$(L^2(\Omega))^2 = \mathbf{H}(\operatorname{div}, 0) \perp \mathbf{H}(\operatorname{div}, 0)^\perp$$

Divergence-free:  $\mathbf{H}(\operatorname{div}, 0) := \{\vec{v} \in (L^2(\Omega))^2 \mid \operatorname{div} \vec{v} = 0, \vec{v} \cdot \vec{n}|_\Gamma = 0\}$

Curl-free:  $\mathbf{H}(\operatorname{div}, 0)^\perp = \{\nabla p \mid p \in H^1(\Omega)\}$



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### Leray Projector $P$

This splitting is equivalent to  $\vec{v} = \vec{v}_{\operatorname{div},0} + \nabla p$ , where  $\vec{v}_{\operatorname{div},0}$  and  $p$  fulfill

$$\vec{v}_{\operatorname{div},0} + \nabla p = \vec{v} \quad \text{in } \Omega,$$

$$\operatorname{div} \vec{v}_{\operatorname{div},0} = 0 \quad \text{in } \Omega,$$

$$\vec{v}_{\operatorname{div},0} \cdot \vec{n} = 0 \quad \text{on } \Gamma.$$

$P : (L^2(\Omega))^2 \rightarrow \mathbf{H}(\operatorname{div}, 0)$  with  $P : \vec{v} \mapsto \vec{v}_{\operatorname{div},0}$ .





### Projection Method

[HEINKENSCHLOSS/SORENSEN/SUN '08]

- Index reduction for Lyapunov-solver.
- Projector:

$$\Pi^T := I_{n_v} - M_v^{-1} G (G^T M_v^{-1} G)^{-1} G^T.$$



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Recall  $P : \vec{v} \mapsto \vec{w}$ :

$$\begin{aligned} \vec{w} + \nabla p &= \vec{v}, \\ \operatorname{div} \vec{w} &= 0 \end{aligned} \quad \Rightarrow \quad \begin{bmatrix} M_v & G \\ G^T & 0 \end{bmatrix} \begin{bmatrix} \mathbf{w} \\ \mathbf{p} \end{bmatrix} = \begin{bmatrix} M_v \mathbf{v} \\ 0 \end{bmatrix}$$

$$\mathbf{p} = (G^T M_v^{-1} G)^{-1} G^T \mathbf{v}$$

$$\mathbf{w} = (I_{n_v} - M_v^{-1} G (G^T M_v^{-1} G)^{-1} G^T) \mathbf{v}$$



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Leray vs.  $\Pi^T$

$$\begin{aligned} \vec{w} &= P(\vec{v}), & \mathbf{w} &= \Pi^T \mathbf{v}, \\ 0 &= \operatorname{div} \vec{w} & \Rightarrow & 0 = G^T \mathbf{w} \end{aligned}$$



Minimize

$$\mathcal{J}(\mathbf{y}, \mathbf{u}) = \frac{1}{2} \int_0^\infty \lambda^2 \|\mathbf{y}\|^2 + \|\mathbf{u}\|^2 \, dt$$

subject to

$$\hat{\Theta}_r^T M \hat{\Theta}_r \frac{d}{dt} \tilde{\mathbf{x}}(t) = \hat{\Theta}_r^T A \hat{\Theta}_r \tilde{\mathbf{x}}(t) + \hat{\Theta}_r^T B \mathbf{u}(t)$$

$$\mathbf{y}(t) = C \hat{\Theta}_r \tilde{\mathbf{x}}(t)$$

with  $\hat{\Pi} = \hat{\Theta}_l \hat{\Theta}_r^T$  such that  $\hat{\Theta}_r^T \hat{\Theta}_l = I \in \mathbb{R}^{(n-n_p) \times (n-n_p)}$  and  $\tilde{\mathbf{x}} = \hat{\Theta}_l^T \mathbf{x}$ .



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$$\mathcal{J}(\mathbf{y}, \mathbf{u}) = \frac{1}{2} \int_0^\infty \lambda^2 \|\mathbf{y}\|^2 + \|\mathbf{u}\|^2 \, dt$$

subject to

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with  $\mathcal{M} = \mathcal{M}^T \succ 0$ .



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### Riccati Based Feedback Approach

- Optimal control:  $\mathbf{u}(t) = -\mathcal{K} \tilde{\mathbf{x}}(t)$ , with feedback:  $\mathcal{K} = \mathcal{B}^T \mathcal{X} \mathcal{M}$ , where  $\mathcal{X}$  is the solution of the generalized continuous-time algebraic Riccati equation (GCARE)

$$\mathcal{R}(\mathcal{X}) = \lambda^2 \mathcal{C}^T \mathcal{C} + \mathcal{A}^T \mathcal{X} \mathcal{M} + \mathcal{M} \mathcal{X} \mathcal{A} - \mathcal{M} \mathcal{X} \mathcal{B} \mathcal{B}^T \mathcal{X} \mathcal{M} = 0.$$



Determine  $\mathcal{X} = \mathcal{X}^T \succeq 0$  such that  $\mathcal{R}(\mathcal{X}) = \mathcal{C}^T \mathcal{C} + \mathcal{A}^T \mathcal{X} \mathcal{M} + \mathcal{M} \mathcal{X} \mathcal{A} - \mathcal{M} \mathcal{X} \mathcal{B} \mathcal{B}^T \mathcal{X} \mathcal{M} = 0$ .



# Feedback Stabilization for Index-2 DAE Systems

## — Nested Iteration without Projection —

Determine  $\mathcal{X} = \mathcal{X}^T \succeq 0$  such that  $\mathcal{R}(\mathcal{X}) = \mathcal{C}^T \mathcal{C} + \mathcal{A}^T \mathcal{X} \mathcal{M} + \mathcal{M} \mathcal{X} \mathcal{A} - \mathcal{M} \mathcal{X} \mathcal{B} \mathcal{B}^T \mathcal{X} \mathcal{M} = 0$ .

Kleinman–Newton method





Determine  $\mathcal{X} = \mathcal{X}^T \succeq 0$  such that  $\mathcal{R}(\mathcal{X}) = \mathcal{C}^T \mathcal{C} + \mathcal{A}^T \mathcal{X} \mathcal{M} + \mathcal{M} \mathcal{X} \mathcal{A} - \mathcal{M} \mathcal{X} \mathcal{B} \mathcal{B}^T \mathcal{X} \mathcal{M} = 0$ .

**Step  $m + 1$ :** Solve the Lyapunov equation

$$(\mathcal{A} - \mathcal{B} \mathcal{K}^{(m)})^T \mathcal{X}^{(m+1)} \mathcal{M} + \mathcal{M} \mathcal{X}^{(m+1)} (\mathcal{A} - \mathcal{B} \mathcal{K}^{(m)}) = -(\mathcal{W}^{(m)})^T \mathcal{W}^{(m)} \quad (1)$$



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Kleinman–Newton method

low-rank ADI method



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**Step  $\ell$ :** Solve the projected and shifted linear system

$$(\mathcal{A} - \mathcal{B} \mathcal{K}^{(m)} + q_\ell \mathcal{M})^T \mathcal{V}_\ell = \mathcal{Y} \quad (2)$$

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**Replace (2) and solve instead** the saddle point system (SPS)

$$\begin{bmatrix} A^T - (K^{(m)})^T B^T + q_\ell M & \hat{G} \\ \hat{G}^T & 0 \end{bmatrix} \begin{bmatrix} \mathcal{V}_\ell \\ * \end{bmatrix} = \begin{bmatrix} \mathcal{Y} \\ 0 \end{bmatrix}$$

for different ADI shifts  $q_\ell \in \mathbb{C}^-$  for a couple of rhs  $\mathcal{Y}$ .

Kleinman–Newton method

low-rank ADI method

linear solver



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(using *Sherman–Morrison–Woodbury* formula)

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for different ADI shifts  $q_\ell \in \mathbb{C}^-$  for a couple of rhs  $\tilde{\mathcal{Y}}$ .





### Theorem

[B./Heinkenschloss/Saak/Weichelt '16]

- assume  $(\mathbf{A}, \mathbf{B}; \mathbf{M})$  stabilizable,  $(\mathbf{C}, \mathbf{A}; \mathbf{M})$  detectable
- $\Rightarrow \exists$  unique, symmetric solution  $X^{(*)} = \hat{\Theta}_r \mathcal{X}^{(*)} \hat{\Theta}_r^T$  with  $\mathcal{R}(\mathcal{X}^{(*)}) = 0$  that stabilizes

$$\left( \begin{bmatrix} A - BB^T X^{(*)} M & \hat{G} \\ \hat{G}^T & 0 \end{bmatrix}, \begin{bmatrix} M & 0 \\ 0 & 0 \end{bmatrix} \right)$$

- for  $\{X^{(k)}\}_{k=0}^{\infty}$  defined by  $X^{(k)} := \hat{\Theta}_r \mathcal{X}^{(k)} \hat{\Theta}_r^T$ , (1), and  $X^{(0)}$  symmetric with  $(\mathbf{A} - \mathbf{B} (\mathbf{K}^{(0)})^T, \mathbf{M})$  stable, it holds that, for  $k \geq 1$ ,

$$X^{(1)} \succeq X^{(2)} \succeq \dots \succeq X^{(k)} \succeq 0 \quad \text{and} \quad \lim_{k \rightarrow \infty} X^{(k)} = X^{(*)}$$

- $\exists 0 < \tilde{\kappa} < \infty$  such that, for  $k \geq 1$ ,

$$\|X^{(k+1)} - X^{(*)}\|_F \leq \tilde{\kappa} \|X^{(k)} - X^{(*)}\|_F^2$$



# Feedback Stabilization for Index-2 DAE Systems

## — Remarks/Open Problems —

### Additional Contributions

[Bänsch/B./Saak/Weichelt '15,'16]

- Suitable approximation framework for Raymond's projected boundary control input.
- Proposed method directly iterates on the feedback matrix  $K \in \mathbb{R}^{n \times n_r}$ .
- Initial feedback for index-2 DAE systems using a special eigenvalue shifting technique.
- Improved ADI shift computation for index-2 DAE systems (Penzl- and projection shifts).



## Additional Contributions

[Bänsch/B./Saak/Weichelt '15,'16]

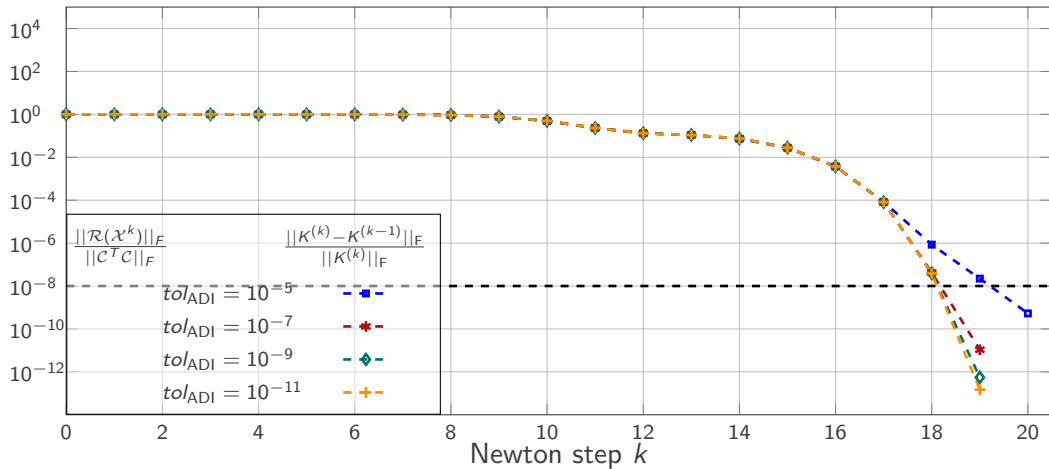
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## Current Problems

- Determination of suitable stopping criteria/tolerances.
- Computation of projected residuals is very costly ( $\approx 10\times$  ADI step).  
 $\Rightarrow$  use relative change of feedback matrix [B./LI/PENZL '08]

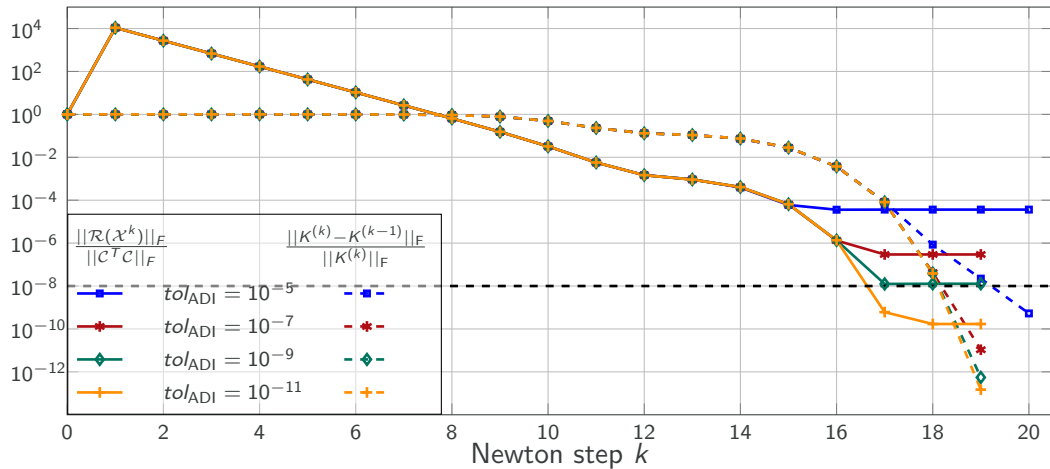


NSE scenario:  $Re = 500$ ,  $n = 5468$ ,  $\lambda = 10^2$ ,  $tol_{\text{Newton}} = 10^{-8}$





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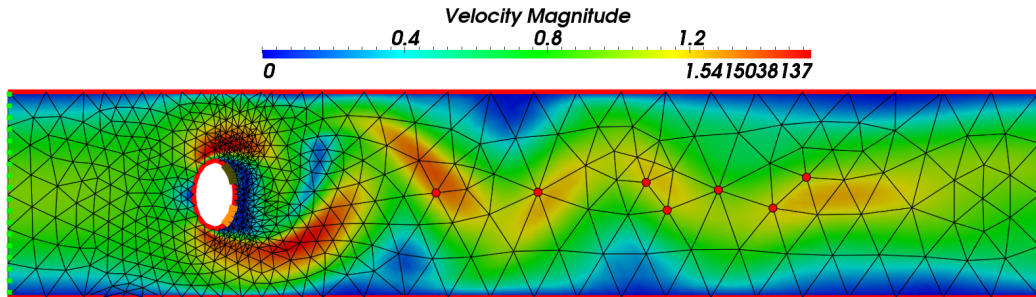


1. Introduction
2. Feedback Stabilization for Index-2 DAE Systems
3. Accelerated Solution of Riccati Equations
4. Conclusions

- Coefficients of GCARE are large-scale matrices (resulting from FE discretization).
- Quadratic system matrices  $A$ ,  $M = M^T \in \mathbb{R}^{n \times n}$  are sparse.

$$\mathcal{R}(X) = C^T C + A^T X M + M X A - M X B B^T X M$$

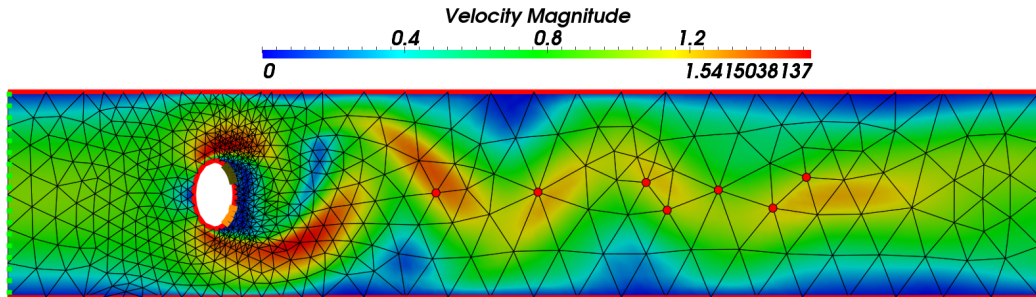
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$$\square = \text{---} + \text{///} \square \text{///} + \text{///} \square \text{///} - \text{///} \square \text{---} \square \text{---} \text{///}$$

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- Residual is of low rank;  $R(ZZ^T) = WW^T$ ,  $W \in \mathbb{R}^{n \times k}$ ,  $k \leq 2n_r + n_a \ll n$

$$WW^T = C^T C + A^T ZZ^T M + MZZ^T A - MZZ^T BB^T ZZ^T M$$

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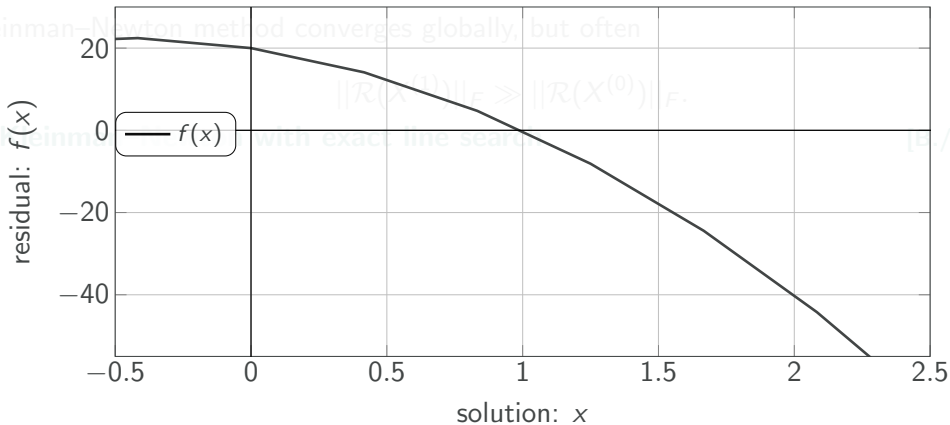


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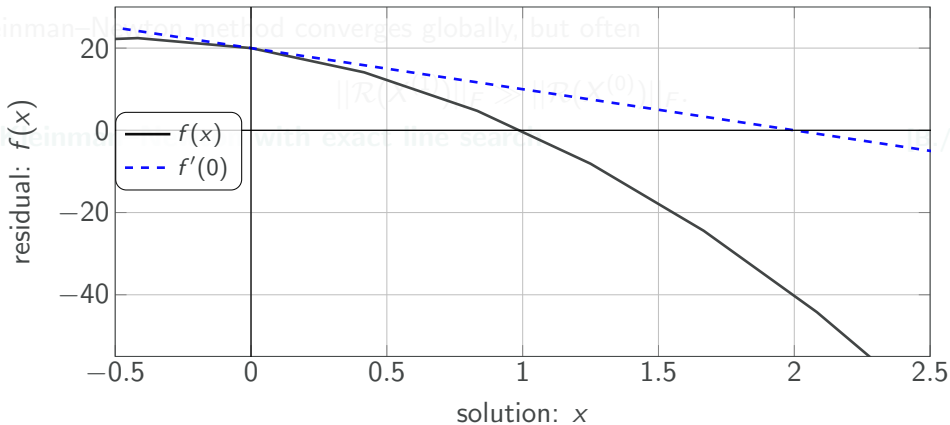


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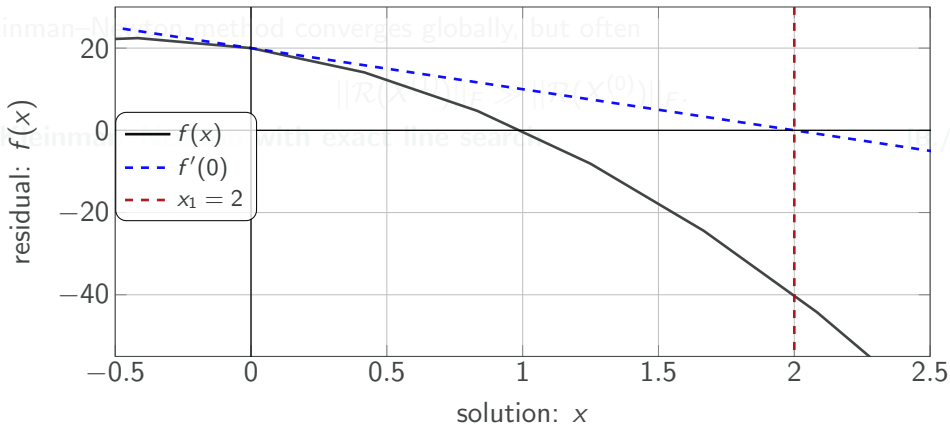


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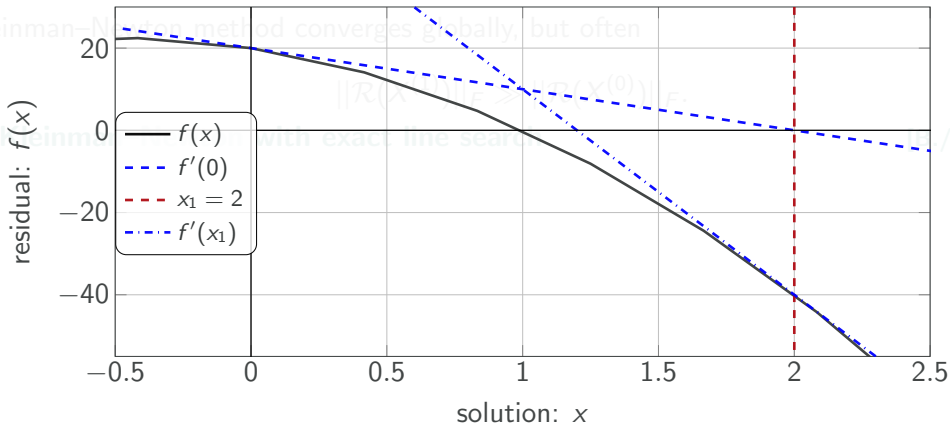


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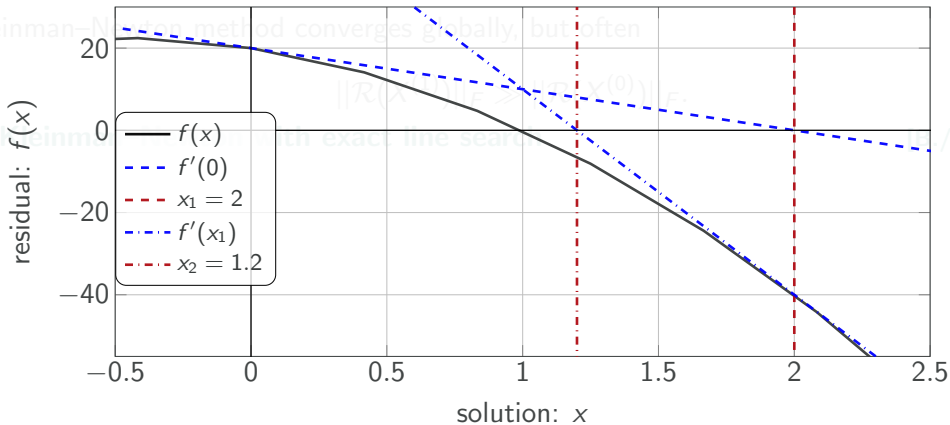


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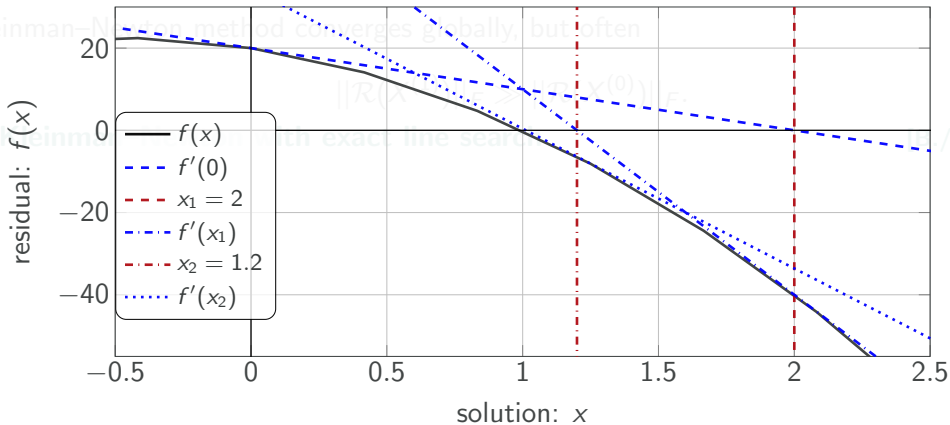


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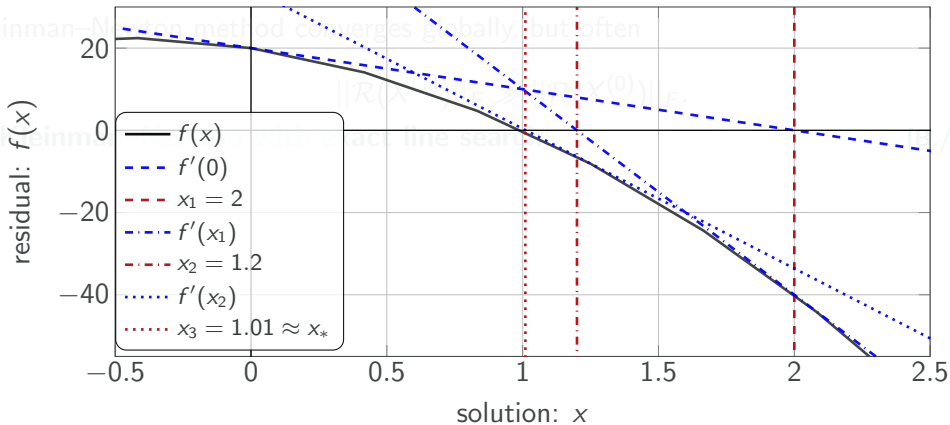


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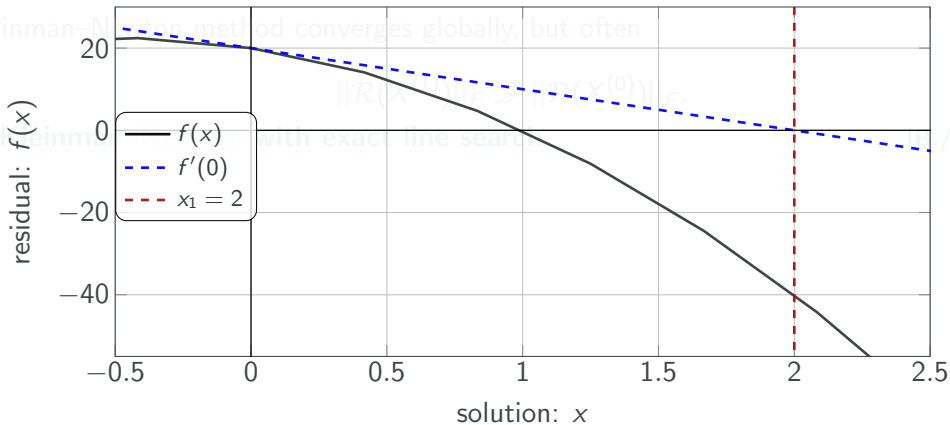


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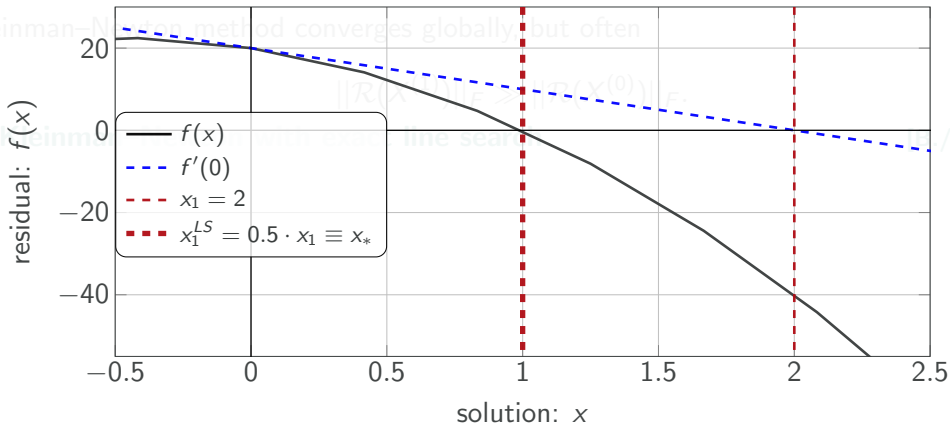


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- **extension to index-2 DAE case “straight forward”**

**Theorem****[B./Heinkenschloss/Saak/Weichelt '16]**

Set  $\tau_k \in (0, 1)$  and assume:  $(\mathcal{A}, \mathcal{B}; \mathcal{M})$  stabilizable,  $(\mathcal{C}, \mathcal{A}; \mathcal{M})$  detectable, and  $\exists \tilde{\mathcal{X}}^{(k+1)} \succeq 0 \forall k$  that solves

$$(\mathcal{A} - \mathcal{B}\mathcal{K}^{(k)})^T \tilde{\mathcal{X}}^{(k+1)} \mathcal{M} + \mathcal{M} \tilde{\mathcal{X}}^{(k+1)} (\mathcal{A} - \mathcal{B}\mathcal{K}^{(k)}) = -\mathcal{C}^T \mathcal{C} - (\mathcal{K}^{(k)})^T \mathcal{K}^{(k)} + \mathcal{L}^{(k+1)}$$

such that

$$\|\mathcal{L}^{(k+1)}\|_F \leq \tau_k \|\mathcal{R}(\mathcal{X}^{(k)})\|_F.$$

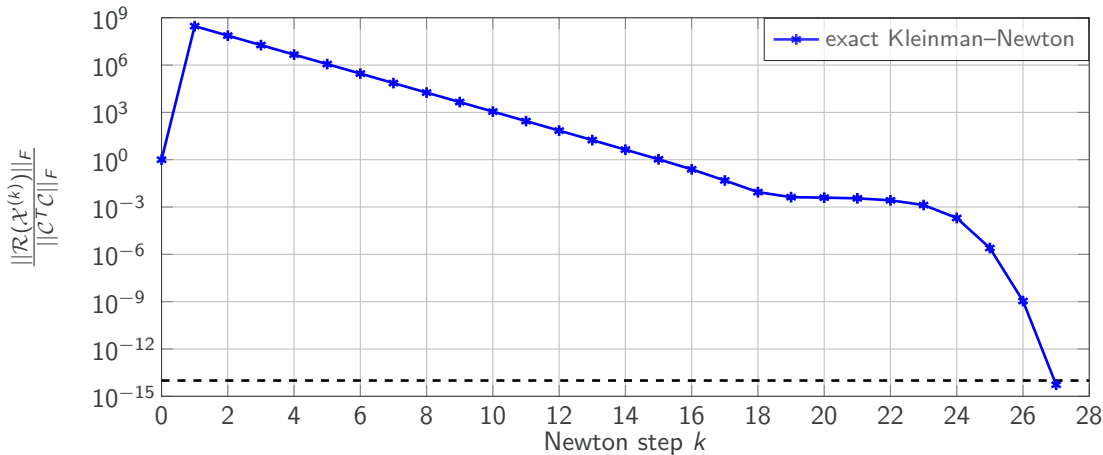
Find  $\xi_k \in (0, 1]$  such that  $\|\mathcal{R}(\mathcal{X}^{(k)} + \xi_k \mathcal{S}^{(k)})\|_F \leq (1 - \xi_k \alpha) \|\mathcal{R}(\mathcal{X}^{(k)})\|_F$  and set

$$\mathcal{X}^{(k+1)} = (1 - \xi_k) \mathcal{X}^{(k)} + \xi_k \tilde{\mathcal{X}}^{(k+1)}.$$

- 1 IF**  $\xi_k \geq \xi_{\min} > 0 \forall k \Rightarrow \|\mathcal{R}(\mathcal{X}^{(k)})\|_F \rightarrow 0$ .
- 2 IF**  $\mathcal{X}^{(k)} \succeq 0$ , and  $(\mathcal{A} - \mathcal{B}\mathcal{B}^T \mathcal{X}^{(k)}, \mathcal{M})$  stable for  $k \geq K > 0 \Rightarrow \mathcal{X}^{(k)} \rightarrow \mathcal{X}^{(*)}$   
 $(\mathcal{X}^{(*)} \succeq 0$  the unique stabilizing solution).



NSE scenario:  $Re = 500$ , Level 1,  $\lambda = 10^4$ ,  $tol_{\text{Newton}} = 10^{-14}$

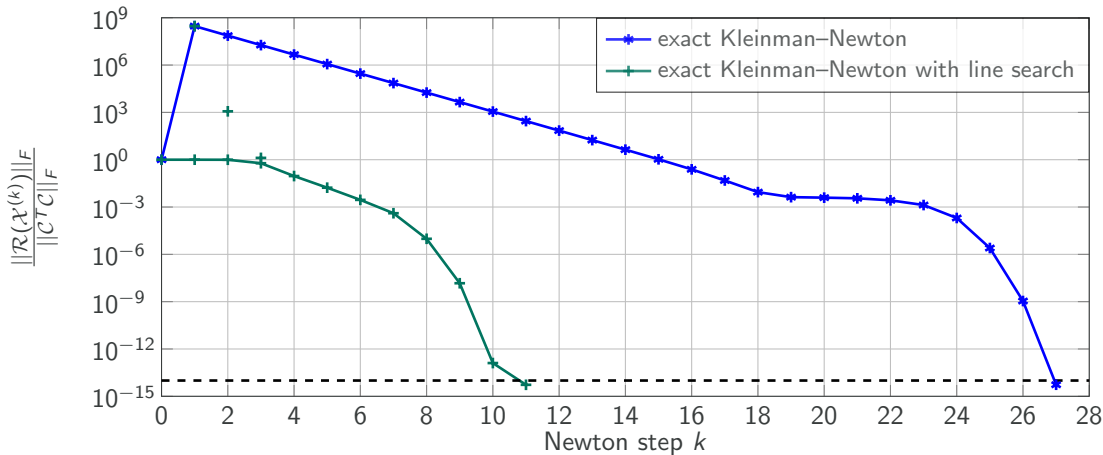




# Accelerated Solution of Riccati Equations

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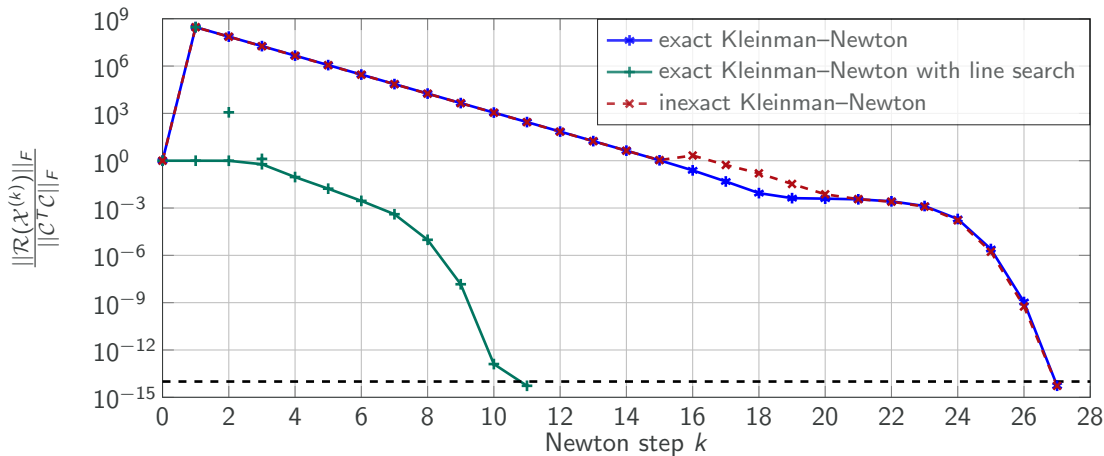




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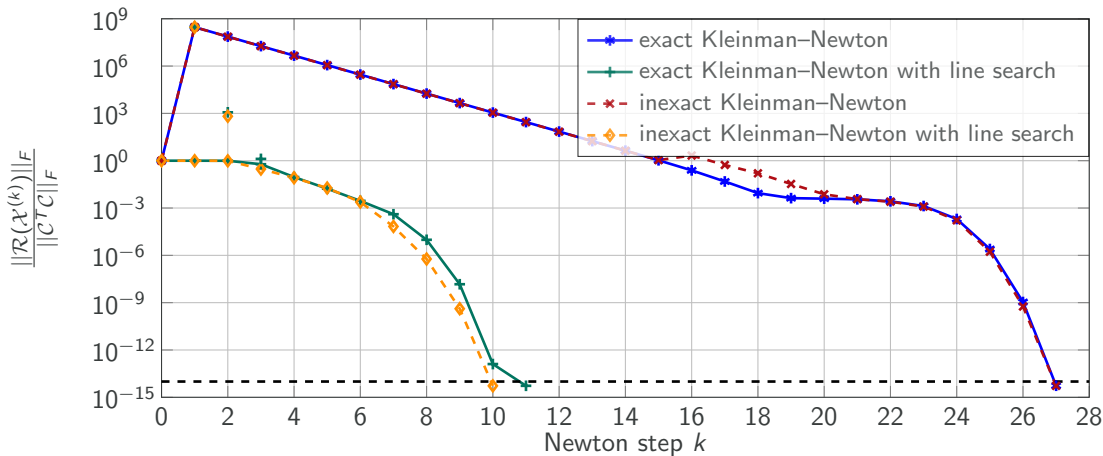




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$\#Newt$	27	11	27	10
$\#ADI$	3185	1351	852	549
$t_{\text{Newt-ADI}}$	1304.769	540.984	331.871	222.295
$t_{\text{shift}}$	29.998	12.568	7.370	5.507
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Table: Numbers of steps and timings in seconds.



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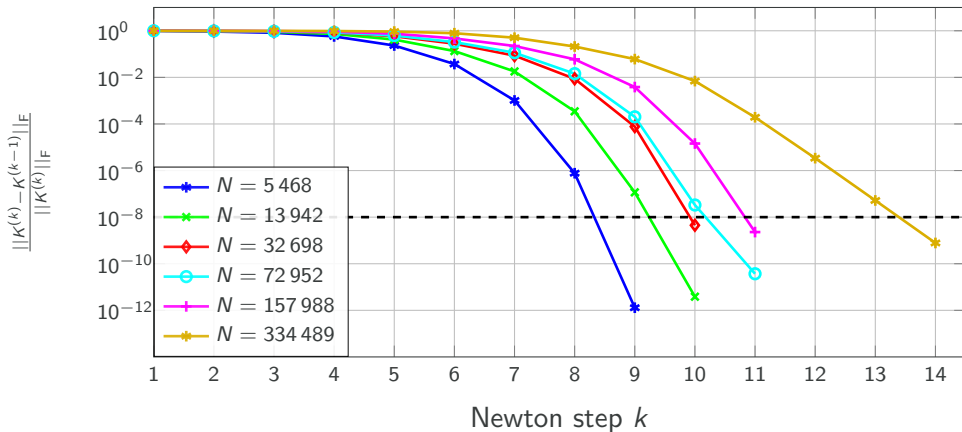
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# Accelerated Solution of Riccati Equations Feedback Stabilization for Index-2 DAE systems

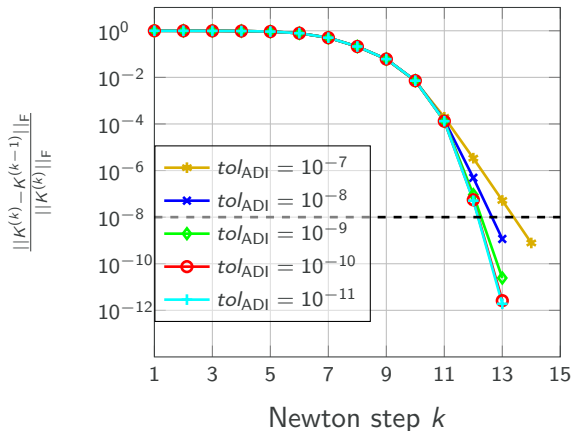
NSE scenario:  $\text{Re} = 500$ ,  $\text{tol}_{\text{ADI}} = 10^{-7}$ ,  $\text{tol}_{\text{Newton}} = 10^{-8}$





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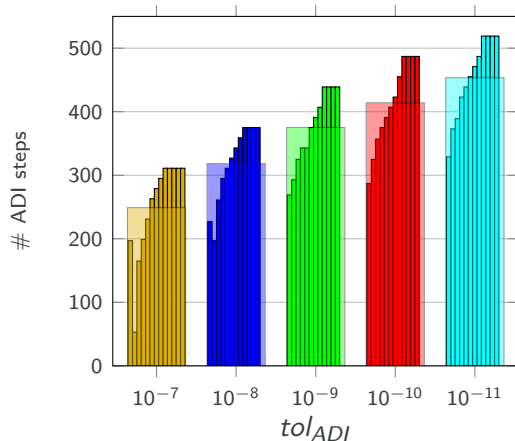
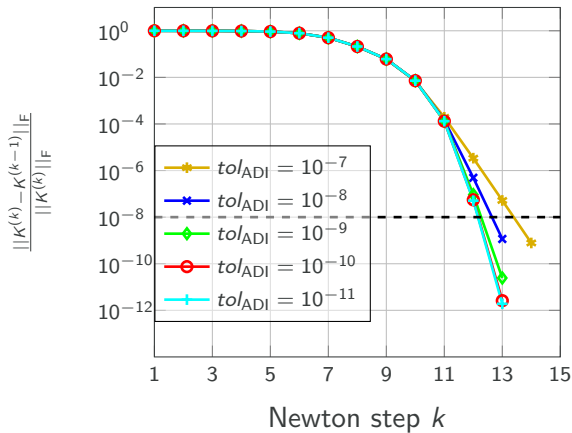
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## Main Contributions

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- Wide-spread usability tailored for standard **inf-sup stable finite element** discretizations.
- Established **specially tailored Kleinman–Newton-ADI** that **avoids explicit projections**.
- **Suitable preconditioners** for multi-field flow problems have been developed.
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⇒ Showed **overall usability** of new approach by a **closed-loop forward simulation**.



-  E. BÄNSCH AND P. BENNER, *Stabilization of incompressible flow problems by Riccati-based feedback*, in *Constrained Optimization and Optimal Control for Partial Differential Equations*, vol. 160 of *International Series of Numerical Mathematics*, Birkhäuser, 2012, pp. 5–20.
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