

MAX PLANCK INSTITUTE FOR DYNAMICS OF COMPLEX TECHNICAL SYSTEMS MAGDEBURG



COMPUTATIONAL METHODS IN SYSTEMS AND CONTROL THEORY

Computational Methods for Feedback Control of Flow Problems **Björn Baran Peter Benner** Jens Saak **Heiko Weichelt** on Numerical Analysis and Scientific Computing the occasion of Prof. Eberhard Bänsch's 60th birthday Erlangen, 22-23 November 2019 Supported by: DFG 😁



Mainly working on



Mainly working on

Schäufele





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- Schäufele
- St. Emilion





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- rivalry of SVW vs. FCB.





VS.



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Chemnitz/Magdeburg – Erlangen, 2005 – 2013

Eventually, some idea of joint work evolved around call for proposals within DFG Priority Program 1253 Optimization with Partial Differential Equations . . .



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Chemnitz/Magdeburg – Erlangen, 2005 – 2013

Eventually, some idea of joint work evolved around call for proposals within DFG Priority Program 1253 Optimization with Partial Differential Equations . . .

stabilization and feedback control of multi-field flow problems!



Our joint proposal for SPP1253 ... Chemnitz, October 12, 2005 (a few days before the deadline)

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Our joint proposal for SPP1253 ... hard at work



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- Physical transport is one of the most fundamental dynamical processes in nature.
- Prediction and manipulation of transport processes are important research topics, e.g., to
 - avoid stall for stable and safe flight;
 - save energy (or increase attainable speed) by minimizing drag coefficient;
 - use fluid flow for optimal transport (e.g., in blood veins).
- **Open-loop** controllers are widely used in various engineering fields. \rightarrow **Not robust** regarding perturbation
- Dynamical systems are often influenced via so called distributed control.
 - \rightarrow Unfeasible in many real-world areas

 \Rightarrow Boundary feedback stabilization (closed-loop) can be used to increase robustness and feasibility.



Let (x_*, u_*) solve $\min_{u \in \mathcal{U}_{ad}} J(x, u)$ s.t. $\dot{x}(t) = f(x(t), u(t))$.



Let
$$(x_*, u_*)$$
 solve $\min_{u \in \mathcal{U}_{ad}} J(x, u)$ s.t. $\dot{x}(t) = f(x(t), u(t))$.

Fundamental observation

Optimized trajectory $x_*(t; u_*)$ and precomputed optimal control $u_*(t)$ will not be attainable in practice due to

- modeling errors and/or unmodeled dynamics,
- model uncertainties,
- external perturbations,
- measurement errors.



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- model uncertainties,
- external perturbations,
- measurement errors.

Consequence: for compensation of errors and correction of deviation from desired path, need feedback control

$$u(t) = u_*(t) + U(t, x(t) - x_*(t)).$$



- Consider 2D flow problems described by incompressible Navier–Stokes equations.
- Riccati feedback approach requires the solution of an algebraic Riccati equation.
- Conservation of mass introduces a **divergence-freeness** condition ~→ problems with mathematical basis of control design schemes.



Kármán vortex street



- Consider 2D flow problems described by incompressible Navier–Stokes equations.
- Riccati feedback approach requires the solution of an algebraic Riccati equation.
- Conservation of mass introduces a **divergence-freeness** condition ~→ problems with mathematical basis of control design schemes.
- **Coupling** flow problems with a scalar reaction-advection-diffusion equation.







Establish a numerical realization for Leray projection.



Establish a numerical realization for Leray projection.

2. NAVIER: FE package using \mathcal{P}_2 - \mathcal{P}_1 Taylor–Hood elements.



- Functional analytic control approach by Raymond ([RAYMOND '05-'07]) works in subspace of divergence-free functions.
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Develop techniques to deal with complex-shifted multi-field flow











Feedback Stabilization for Projected Systems After Leray-projecting the system equations... (and three years later)

Minimize

$$\mathcal{J}(\mathbf{y},\mathbf{u}) = \frac{1}{2} \int_0^\infty \lambda^2 ||\mathbf{y}||^2 + ||\mathbf{u}||^2 \mathrm{\,d} t$$

subject to

$$\begin{split} \widehat{\Theta}_r^T M \widehat{\Theta}_r \frac{\mathsf{d}}{\mathsf{d}t} \widetilde{\mathbf{x}}(t) &= \widehat{\Theta}_r^T A \widehat{\Theta}_r \widetilde{\mathbf{x}}(t) + \widehat{\Theta}_r^T B \mathbf{u}(t) \\ \mathbf{y}(t) &= C \widehat{\Theta}_r \widetilde{\mathbf{x}}(t) \\ \end{split}$$
 with $\widehat{\Pi} &= \widehat{\Theta}_l \widehat{\Theta}_r^T$ such that $\widehat{\Theta}_r^T \widehat{\Theta}_l = I \in \mathbb{R}^{(n-n_{\mathbf{p}}) \times (n-n_{\mathbf{p}})}$ and $\widetilde{\mathbf{x}} = \widehat{\Theta}_l^T \mathbf{x}.$



Feedback Stabilization for Projected Systems After Leray-projecting the system equations... (and three years later)

Minimize

$$\mathcal{J}(\mathbf{y},\mathbf{u}) = \frac{1}{2}\int_0^\infty \lambda^2 ||\mathbf{y}||^2 + ||\mathbf{u}||^2 \mathrm{\,d} t$$

subject to

$$\mathcal{M}\frac{\mathsf{d}}{\mathsf{d}t}\widetilde{\boldsymbol{x}}(t) = \mathcal{A}\widetilde{\boldsymbol{x}}(t) + \mathcal{B}\mathbf{u}(t)$$
$$\mathbf{y}(t) = \mathcal{C}\widetilde{\boldsymbol{x}}(t)$$

with $\mathcal{M} = \mathcal{M}^T \succ 0$.



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subject to

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$$\mathbf{y}(t) = \mathcal{C}\widetilde{\boldsymbol{x}}(t)$$

with $\mathcal{M} = \mathcal{M}^T \succ 0$.

Riccati Based Feedback Approach

• Optimal control: $\mathbf{u}(t) = -\mathcal{K}\widetilde{\mathbf{x}}(t)$, with feedback: $\mathcal{K} = \mathcal{B}^T \mathcal{X} \mathcal{M}$,

where ${\cal X}$ is the solution of the generalized continuous-time algebraic Riccati equation (GCARE)

$$\mathcal{R}(\mathcal{X}) = \lambda^2 \mathcal{C}^T \mathcal{C} + \mathcal{A}^T \mathcal{X} \mathcal{M} + \mathcal{M} \mathcal{X} \mathcal{A} - \mathcal{M} \mathcal{X} \mathcal{B} \mathcal{B}^T \mathcal{X} \mathcal{M} = 0.$$



- Analyzed Riccati-based feedback for scalar and vector-valued transport problems.
- Wide-spread usability tailored for standard inf-sup stable finite element discretizations.
- Established specially tailored Kleinman–Newton-ADI that avoids explicit projections.
- **Suitable preconditioners** for multi-field flow problems have been developed.
- Major run time improvements due to combination of inexact Newton and line search.
- Established new convergence proofs that were verified by extensive numerical tests.
- $\blacksquare \Rightarrow$ Showed usability of new approach by a closed-loop forward simulation.



Project Output so far...

E. BÄNSCH AND P. BENNER, Stabilization of incompressible flow problems by Riccati-based feedback, in Constrained Optimization and Optimal Control for Partial Differential Equations, vol. 160 of International Series of Numerical Mathematics, Birkhäuser, 2012, pp. 5–20.



P. BENNER, J. SAAK, M. STOLL, AND H. K. WEICHELT, *Efficient solution of large-scale saddle point systems arising in Riccati-based boundary feedback stabilization of incompressible Stokes flow*, **SIAM J. Sci. Comput.**, 35 (2013), pp. S150–S170.



E. BÄNSCH, P. BENNER, J. SAAK, AND H. K. WEICHELT, *Optimal control-based feedback stabilization of multi-field flow problems*, in Trends in PDE Constrained Optimization, vol. 165 of Internat. Ser. Numer. Math., Birkhäuser, Basel, 2014, pp. 173–188.



E. BÄNSCH, P. BENNER, J. SAAK, AND H. K. WEICHELT, *Riccati-based boundary feedback stabilization of incompressible Navier-Stokes flows*, SIAM J. Sci. Comput., 37 (2015), pp. A832–A858.

P. BENNER, M. HEINKENSCHLOSS, J. SAAK, AND H. K. WEICHELT, *Efficient solution of large-scale algebraic Riccati equations associated with index-2 DAEs via the inexact low-rank Newton-ADI method*, **Appl. Numer. Math.**, accepted 2019-11-21 (2019).









I.e., we promised to stabilize the interface at solid/liquid phase transitions with convection \ldots





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The first birthday present: It's (partially) done!





l.e., we promised to stabilize the interface at solid/liquid phase transitions with convection \ldots

- The first birthday present: It's (partially) done!
- Rest of the talk: feedback control of the Stefan problem.


Linear Quadratic Regulator

Stefan Problem

Structural Properties

Numerical Examples

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Motivation Feedback Stabilization of the Heat Equation with Riccati-feedback

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CSC

Minimize
$$\begin{aligned} &\frac{1}{2} \int_{0}^{t_{f}} \lambda \left\| \theta - \theta_{d} \right\|^{2} + \left\| \mathbf{u} \right\|^{2} \ dt \\ \text{subject to} \\ &\frac{d}{dt} \theta - k \Delta \theta = 0, \qquad \Omega \\ &g(\theta) = \mathbf{u}, \qquad \partial \Omega \end{aligned}$$

Motivation Feedback Stabilization of the Heat Equation with Riccati-feedback

| Ω | |
|---|--|
| | |

CSC

Minimize
$$\frac{1}{2} \int_{0}^{t_{f}} \lambda \|y - y_{d}\|^{2} + \|\mathbf{u}\|^{2} dt$$

subject to
$$\frac{d}{dt} \theta - k\Delta\theta = 0, \qquad \Omega$$
$$g(\theta) = \mathbf{u}, \qquad \partial\Omega$$

Discretization:
$$A, M \text{ large sparse, } B, C \text{ skinny}$$
$$M\dot{x} = Ax + B\mathbf{u}$$
$$y = Cx$$



$$M\dot{x} = Ax + B\mathbf{u}$$
$$y = Cx$$

Riccati-based Feedback Approach

e.g.,[SONTAG '98]

• Stabilizing feedback: $\mathcal{K} = \mathcal{B}^{\mathsf{T}} \mathbf{X} \mathcal{M}$

where ${\bf X}$ is the solution of the generalized differential Riccati equation (DRE)

$$-\mathcal{M}^{\mathsf{T}}\dot{\mathbf{X}}\mathcal{M} = \mathcal{C}^{\mathsf{T}}\mathcal{C} + \mathcal{A}^{\mathsf{T}}\mathbf{X}\mathcal{M} + \mathcal{M}^{\mathsf{T}}\mathbf{X}\mathcal{A} - \mathcal{M}^{\mathsf{T}}\mathbf{X}\mathcal{B}\mathcal{B}^{\mathsf{T}}\mathbf{X}\mathcal{M}$$

• Optimal control: $\mathbf{u} = -\mathcal{K}x$



$-\mathcal{M}^{\mathsf{T}}\dot{\mathbf{X}}\mathcal{M} = \mathcal{C}^{\mathsf{T}}\mathcal{C} + \mathcal{A}^{\mathsf{T}}\mathbf{X}\mathcal{M} + \mathcal{M}^{\mathsf{T}}\mathbf{X}\mathcal{A} - \mathcal{M}^{\mathsf{T}}\mathbf{X}\mathcal{B}\mathcal{B}^{\mathsf{T}}\mathbf{X}\mathcal{M}$ $\mathbf{X} \approx ZZ^{\mathsf{T}} \quad \text{or} \quad \mathbf{X} \approx LDL^{\mathsf{T}}$

- Backward Differentiation Formula (BDF)
- Rosenbrock

. . .

- Peer methods
- Splitting schemes
- Krylov subspace methods

[Behr/Benner/Heiland '18, Kirsten/Simoncini '19, Koskela/Mena '18, Lang '17, Mena '07, Ostermann/Piazzola/Walach '18, Stillfjord '15, Stillfjord '18, ...]





Time dependent heat conductivity k(t)

$$\frac{d}{dt}\theta - \mathbf{k}(t)\Delta\theta = 0, \qquad \Omega$$
$$g(\theta) = \mathbf{u}, \qquad \partial\Omega$$

$$M\dot{x} = A(t)x + B\mathbf{u}$$
$$y = Cx$$
$$A(t) = k(t)A_0 \qquad k \colon \mathbb{R} \to \mathbb{R}$$



$-\mathcal{M}^{\mathsf{T}}\dot{\mathbf{X}}\mathcal{M} = \mathcal{C}^{\mathsf{T}}\mathcal{C} + \mathcal{A}(t)^{\mathsf{T}}\mathbf{X}\mathcal{M} + \mathcal{M}^{\mathsf{T}}\mathbf{X}\mathcal{A}(t) - \mathcal{M}^{\mathsf{T}}\mathbf{X}\mathcal{B}\mathcal{B}^{\mathsf{T}}\mathbf{X}\mathcal{M}$ $\mathbf{X} \approx LDL^{\mathsf{T}}$

BDF

- Rosenbrock
- Peer methods

. . .

[Lang '17, Mena '07, ...]



Linear Quadratic Regulator

$$M\dot{x} = Ax + B\mathbf{u}$$
$$y = Cx$$

Stefan Problem



Non-autonomous Problem

Stefan Problem

 Γ_{heat}



$$\begin{split} \frac{d}{dt}\theta - \alpha \Delta \theta &= 0, \qquad \Omega_l \cup \Omega_s \\ [k_s(\nabla \theta)_s - k_l(\nabla \theta)_l] \cdot \boldsymbol{n}_{\text{int}} &= LV_{\text{int}}, \qquad \Gamma_{\text{int}} \\ \theta &= \theta_{\text{cool}}, \qquad \Gamma_{\text{cool}} \\ \partial_{\boldsymbol{n}}\theta &= \mathbf{u}, \qquad \Gamma_{\text{heat}} \end{split}$$



Non-autonomous Problem Stefan Problem

$$\begin{aligned} \frac{d}{dt}\theta - \alpha \Delta \theta &= 0, \qquad \Omega_l \cup \Omega_s \\ [k_s(\nabla \theta)_s - k_l(\nabla \theta)_l] \cdot \boldsymbol{n}_{\text{int}} &= LV_{\text{int}}, \qquad \Gamma_{\text{int}} \\ \theta &= \theta_{\text{cool}}, \qquad \Gamma_{\text{cool}} \\ \partial_{\boldsymbol{n}}\theta &= \mathbf{u}, \qquad \Gamma_{\text{heat}} \end{aligned}$$



Non-autonomous Problem

Stefan Problem

 Γ_{heat}



$$\frac{d}{dt}\theta + v \cdot \nabla \theta - \alpha \Delta \theta = 0, \qquad \qquad \Omega_l \cup \Omega_s$$

$$\begin{split} [k_s(\nabla\theta)_s - k_l(\nabla\theta)_l] \cdot \boldsymbol{n}_{\mathsf{int}} &= LV_{\mathsf{int}}, \qquad \Gamma_{\mathsf{int}} \\ \theta &= \theta_{\mathsf{cool}}, \qquad \Gamma_{\mathsf{cool}} \end{split}$$

$$\partial_{n}\theta = \mathbf{u}, \qquad \Gamma_{\text{heat}}$$

$$\begin{aligned} \frac{d}{dt}v - \eta \Delta v + \nabla p &= 0, \qquad & \Omega_l \\ \nabla \cdot v &= 0, \qquad & \Omega_l \end{aligned}$$

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Non-autonomous Problem Stefan Problem

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$$\frac{d}{dt}\theta + v \cdot \nabla \theta - \alpha \Delta \theta = 0, \qquad \qquad \Omega_l \cup \Omega_s$$

$$\begin{split} [k_s(\nabla \theta)_s - k_l(\nabla \theta)_l] \cdot \boldsymbol{n}_{\text{int}} &= LV_{\text{int}}, \qquad \Gamma_{\text{int}} \\ \theta &= \theta_{\text{cool}}, \qquad \Gamma_{\text{cool}} \\ \partial_{\boldsymbol{n}} \theta &= \mathbf{u}, \qquad \Gamma_{\text{heat}} \end{split}$$

$$\frac{d}{dt}v - \eta \Delta v + \nabla p = 0, \qquad \qquad \Omega_l$$

$$\nabla \cdot v = 0, \qquad \qquad \Omega_l$$



Nonlinear Problem ~> Linearization

- Use open-loop control to compute a reference trajectory.
- Linearize around the reference trajectory.



Nonlinear Problem ~> Linearization

- Use open-loop control to compute a reference trajectory.
- Linearize around the reference trajectory.

Changing Domain ~> Moving Mesh / Remeshing

Non-autonomous system:

$$M(t)\dot{x} = A(t)x + B(t)\mathbf{u}$$
$$y = C(t)x$$



Nonlinear Problem ~> Linearization

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$$y = C(t)x$$

Memory Requirements

- Precompute matrices for every required time step.
- Avoid extra time steps in DRE solvers.



Open-loop control simulation:





Open-loop control simulation:





Autonomous DRE

$$-\mathcal{M}^{\mathsf{T}}\dot{\mathbf{X}}\mathcal{M} = \mathcal{C}^{\mathsf{T}}\mathcal{C} + \mathcal{A}^{\mathsf{T}}\mathbf{X}\mathcal{M} + \mathcal{M}^{\mathsf{T}}\mathbf{X}\mathcal{A} - \mathcal{M}^{\mathsf{T}}\mathbf{X}\mathcal{B}\mathcal{B}^{\mathsf{T}}\mathbf{X}\mathcal{M}$$

Non-autonomous DRE

$$\mathcal{M}=\mathcal{M}(t), \mathcal{A}=\mathcal{A}(t), \mathcal{B}=\mathcal{B}(t), \mathcal{C}=\mathcal{C}(t)$$

$$-\mathcal{M}^{\mathsf{T}}\dot{\mathbf{X}}\mathcal{M} = \mathcal{C}^{\mathsf{T}}\mathcal{C} + (\dot{\mathcal{M}} + \mathcal{A})^{\mathsf{T}}\mathbf{X}\mathcal{M} + \mathcal{M}^{\mathsf{T}}\mathbf{X}(\dot{\mathcal{M}} + \mathcal{A})$$
$$-\mathcal{M}^{\mathsf{T}}\mathbf{X}\mathcal{B}\mathcal{B}^{\mathsf{T}}\mathbf{X}\mathcal{M}$$



BDF Method

- Iow-rank multi-step algorithm to solve DREs
- algebraic Riccati equation in each time step
- main work: solution of shifted systems $(\mathcal{A} + p\mathcal{M})V = W$



BDF Method

- Iow-rank multi-step algorithm to solve DREs
- algebraic Riccati equation in each time step
- main work: solution of shifted systems $(\mathcal{A} + p\mathcal{M})V = W$

Non-autonomous DRE ~ Non-autonomous BDF Method

- start-up with fixed number of very small extra time steps
- cannot reuse data from previous time step
- extra matrix-matrix multiplications in each time step



BDF Method

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- algebraic Riccati equation in each time step
- main work: solution of shifted systems $(\mathcal{A} + p\mathcal{M})V = W$

Non-autonomous DRE \rightsquigarrow Non-autonomous BDF Method

- start-up with fixed number of very small extra time steps
- cannot reuse data from previous time step
- extra matrix-matrix multiplications in each time step

$$\mathcal{C}_{k}^{\mathsf{T}} = \left[\sqrt{\lambda} \mathcal{C}(t_{k})^{\mathsf{T}}, \mathcal{M}(t_{k})^{\mathsf{T}} L_{k-1}, \dots, \mathcal{M}(t_{k})^{\mathsf{T}} L_{k-\wp} \right]$$

 $\wp : \text{order of the BDF method}$



Linear Quadratic Regulator









$$x \leftarrow \theta, v \qquad \Gamma \leftarrow V_{\text{int}} \qquad \Phi \leftarrow p$$





Structural Properties Index-1



e.g., [GUGERCIN, STYKEL, WYATT '13]

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Structural Properties Index-1



e.g., [GUGERCIN, STYKEL, WYATT '13]

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Structural Properties Index-1

$$\begin{bmatrix} M_x & 0 \\ 0 & 0 \end{bmatrix} \frac{d}{dt} \begin{bmatrix} x \\ \Gamma \end{bmatrix} = \begin{bmatrix} A & J \\ G & S \end{bmatrix} \begin{bmatrix} x \\ \Gamma \end{bmatrix} + \mathcal{B}\mathbf{u}$$

S regular : $\Gamma = -S^{-1}Gx$

$$M_x \frac{d}{dt} x = \tilde{A} x + \mathcal{B}\mathbf{u}$$

$$\tilde{A} = A - JS^{-1}G$$

e.g., [GUGERCIN, STYKEL, WYATT '13]

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Structural Properties Index-2



e.g., [GUGERCIN, STYKEL, WYATT '13]

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Structural Properties Index-2

$$\begin{bmatrix} M_x & \mathbf{0} \\ \mathbf{0} & \mathbf{0} \end{bmatrix} \frac{d}{dt} \begin{bmatrix} \mathbf{x} \\ \Phi \end{bmatrix} = \begin{bmatrix} A & \mathbf{J} \\ \mathbf{G} & \mathbf{0} \end{bmatrix} \begin{bmatrix} \mathbf{x} \\ \Phi \end{bmatrix} + \mathcal{B}\mathbf{u}$$

$$\begin{split} J,G \text{ full rank}: \qquad \Pi_l = I - J (GM_x^{-1}J)^{-1}GM_x^{-1}\\ \Pi_r = I - M_x^{-1}J (GM_x^{-1}J)^{-1}G \end{split}$$

e.g., [Gugercin, Stykel, Wyatt '13]



Structural Properties Index-2

$$\begin{bmatrix} M_x & 0 \\ 0 & 0 \end{bmatrix} \frac{d}{dt} \begin{bmatrix} x \\ \Phi \end{bmatrix} = \begin{bmatrix} A & J \\ G & 0 \end{bmatrix} \begin{bmatrix} x \\ \Phi \end{bmatrix} + \mathcal{B}\mathbf{u}$$

$$J,G$$
 full rank :
$$\begin{split} \Pi_l &= I - J(GM_x^{-1}J)^{-1}GM_x^{-1}\\ \Pi_r &= I - M_x^{-1}J(GM_x^{-1}J)^{-1}G \end{split}$$

$$\hat{M}_x \frac{d}{dt} x = \hat{A} x + \hat{\mathcal{B}}\mathbf{u}$$

 $\hat{A} = \Pi_l A \Pi_r \qquad \hat{M}_x = \Pi_l M_x \Pi_r \qquad \hat{\mathcal{B}} = \Pi_l \mathcal{B}$

e.g., [GUGERCIN, STYKEL, WYATT '13]





















Implicit Schur Complement and Projection

Explicit

dense: $O(n^2)$ memory

$$\tilde{A} = A - J_1 S^{-1} G_1$$
$$\hat{A} = \Pi_l \tilde{A} \Pi_r \qquad \hat{M} = \Pi_l M_x \Pi_r$$
$$(\hat{A} + p \hat{M}) V = W \text{ and } \Pi_r V = V$$

Implicit Schur Complement and Projection

Explicit

CSC

dense: $O(n^2)$ memory

$$\tilde{A} = A - J_1 S^{-1} G_1$$
$$\hat{A} = \Pi_l \tilde{A} \Pi_r \qquad \hat{M} = \Pi_l M_x \Pi_r$$
$$(\hat{A} + p \hat{M}) V = W \text{ and } \Pi_r V = V$$

$$\iff$$

Implicit

low-rank sparse: O(n) memory

$$\begin{bmatrix} A + pM_x & J_1 & J_2 \\ G_1 & S & J_3 \\ G_2 & G_3 & 0 \end{bmatrix} \begin{bmatrix} V \\ \Gamma \\ \Phi \end{bmatrix} = \begin{bmatrix} W \\ 0 \\ 0 \end{bmatrix}$$


Linear Quadratic Regulator









Aim: Stabilize the interface position Γ_{int} with $\mathbf{u}_f = -\mathcal{K}x$.

Perturbation: Add $\varphi(t)$ at the cooling boundary.



$$\partial_{n}\theta = \mathbf{u}_{0} + \mathbf{u}_{f}$$

$$\Omega_{l}$$

$$\Gamma_{\text{int}}$$

$$\Omega_{s}$$

 $\theta = \theta_{\mathsf{cool}} + \varphi(t)$

$$\frac{1}{2} \int_0^{t_f} \lambda \|\mathbf{y} - y_d\|^2 + \|\mathbf{u}\|^2 dt$$
$$\lambda = 10^4$$







Numerical Examples Test: Cost <u>Functional Weights</u>





Numerical Examples Test: Cost Functional Weights



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Numerical Examples Test: Cost Functional Weights





Numerical Examples Test: Cost Functional Weights





2 vs 7 Outputs





Test: Output





Test: Curvature





Test: Curvature









Numerical Examples Coupled with Stokes Equations





Numerical Examples Coupled with Stokes Equations





Presented

- Riccati-feedback stabilization of the Stefan problem comes with challenges:
 - Non-linear problem,
 - Time-dependent matrices,
 - Non-autonomous DRE,
 - Differential algebraic structure.
- The quality of the feedback depends on the discretization and cost functional.



Presented

- Riccati-feedback stabilization of the Stefan problem comes with challenges:
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- The quality of the feedback depends on the discretization and cost functional.

Outlook

- Further test feedback performance.
- Implement more sophisticated time integrator.
- Couple with Navier-Stokes equations in the liquid phase.



Happy Birthday!



Happy Birthday!

... et Santé !







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$$\mathcal{M}(t) \qquad \left] \frac{d}{dt} \left[\mathbf{x}(t) \right] = \left[\qquad \mathcal{A}(t) \qquad \right] \left[\mathbf{x}(t) \right] + \mathcal{B}(t)\mathbf{u}(t),$$
$$\mathbf{y} = \left[\qquad \mathcal{C}(t) \qquad \right] \left[\mathbf{x}(t) \right].$$



