

MAX PLANCK INSTITUTE FOR DYNAMICS OF COMPLEX TECHNICAL SYSTEMS MAGDEBURG



COMPUTATIONAL METHODS IN SYSTEMS AND CONTROL THEORY

Reduced-order Modeling Enables Digital Twins for Smart Process Engineering

Peter Benner

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Partners:





They allow

- the simulation for analyzing behavior,
- optimizing design and control synthesis,
- surveillance and prediction,
- continuous improvement of the plant model and its controller.



Overlage Corporation



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The latter require real-time response times!



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ⓒNoria Corporation



CEmerson Electric Co.

Smart process engineering (SmartProSys) requires digital twins of, e.g., chemical reactors.

- This involves mathematical models (mass and energy balances, reaction kinetics,...).
- For high precision, this involves accurate discretizations of systems of nonlinear coupled partial differential equations.
- Real-time demands (but also, optimization and controller design) require fast-to-evaluate surrogate models.



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~ MODEL REDUCTION is enabling technology!



$$\Sigma: \left\{ \begin{array}{rl} \dot{x}(t) &=& f(t,x(t),u(t)), \\ y(t) &=& g(t,x(t),u(t)), \end{array} \right.$$

- states $x(t) \in \mathbb{R}^n$,
- inputs $u(t) \in \mathbb{R}^m$,
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Reduced-Order Model (ROM)

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$$\xrightarrow{u}$$
 $\widehat{\Sigma}$ $\xrightarrow{\widehat{y}}$

Goals:

 $\|y - \hat{y}\| < \mathsf{tolerance} \cdot \|u\|$ for all admissible input signals.



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Linear Time-invariant Systems

Original System

$$\Sigma : \begin{cases} \dot{x}(t) = Ax(t) + Bu(t), \\ y(t) = Cx(t) + Du(t). \end{cases}$$

- states $x(t) \in \mathbb{R}^n$,
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- $E, A \in \mathbb{R}^{n \times n}$
- $B \in \mathbb{R}^{n \times m}$
- $C \in \mathbb{R}^{p \times n}$
- $D \in \mathbb{R}^{p \times m}$
- $x(t) \in \mathbb{R}^n$

- $\hat{E}, \hat{A} \in \mathbb{R}^{r \times r}$
- $\hat{B} \in \mathbb{R}^{r \times m}$
- $\hat{C} \in \mathbb{R}^{p \times r}$
- $\hat{D} \in \mathbb{R}^{p \times m}$
- $\hat{x}(t) \in \mathbb{R}^r$, $r \ll n$



Assumption: trajectory x(t; u) is contained in low-dimensional subspace $\mathcal{V} \subset \mathbb{R}^n$.



 $\operatorname{range}(V) = \mathcal{V}, \quad \operatorname{range}(W) = \mathcal{W}, \quad W^T V = I_r.$

MOR Methods Based on Projection

 $\operatorname{range}(V) = \mathcal{V}, \quad \operatorname{range}(W) = \mathcal{W}, \quad W^T V = I_r.$

Then, with $\hat{x} = W^T x$, we obtain $x \approx V \hat{x} = V W^T x =: \tilde{x}$ so that

 $||x - \tilde{x}|| = ||x - V\hat{x}||.$

CSC

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$$\hat{x} = W^T x, \quad \hat{A} := W^T A V, \quad \hat{B} := W^T B, \quad \hat{C} := C V, \quad (\hat{D} := D).$$

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Extends to nonlinear systems with some effort:

$$\dot{\hat{x}} = W^T f(t, V \hat{x}, u), \hat{y} = g(t, V \hat{x}, u).$$

Needs hyper-reduction if the cost for evaluation of the functions $W^T f, g$ is not reduced!

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Classes of Projection-based MOR Methods

- 1 Modal Truncation
- Rational Interpolation / Moment Matching (Padé-Approximation and (rational) Krylov Subspace Methods)
- Balanced Truncation
- **@** Proper Orthogonal Decomposition (POD) / Principal Component Analysis (PCA)
- **6** Reduced Basis Method
- **6** . . .









MAX: Results considering an inhomogeneous initial condition $T_0 \neq 0$ Results by Julia Vettermann (MiIT/TU Chemnitz)

FE-coupled

| method | red. order tol 10^{-3} | t_{red} |
|--------|--------------------------|-----------|
| 2phase | 196 | 6.5h |
| BTX0 | 174 | 4.5h |

output-coupled

| method | red. order tol 10^{-3} | t_{red} |
|--------|--------------------------|-----------|
| 2phase | 3005 | 2h |
| BTX0 | 2515 | 1.8h |



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|--------|--------------------------|-----------|--------|--------------------------|-----------|
| 2phase | 196 | 6.5h | 2phase | 3005 | 2h |
| BTX0 | 174 | 4.5h | BTX0 | 2515 | 1.8h |

 \rightarrow Required storage for reduced matrices just 1MB!

 \rightarrow Simulation speed-up factors range from \approx 8–2,000.



temperature change in output (16, 0)

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Vettermann, J., Sauerzapf, S., Naumann, A., Beitelschmidt, M., Herzog, R., Benner, P., Saak, J. (2021): Model order reduction methods for coupled machine tool models. MM Science Journal, pp. 4652–4659.



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We need the matrices A, B, C, D to compute the reduced-order model!



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Using proprietary simulation software, we would need to intrude the software to get the matrices \rightsquigarrow intrusive MOR

= learning (compact, surrogate) models from (full, detailed) models.

This is often impossible!



What about the Data?

Assumption: trajectory x(t; u) is contained in low-dimensional subspace $\mathcal{V} \subset \mathbb{R}^n$. Thus, use Galerkin or Petrov-Galerkin-type projection of state-space onto \mathcal{V} (trial space) along complementary subspace \mathcal{W} (test space), where

$$\operatorname{range}(V) = \mathcal{V}, \quad \operatorname{range}(W) = \mathcal{W}, \quad W^T V = I_r.$$

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```
~> non-intrusive MOR
```

= Learning (compact, surrogate) models from data!









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• time domain data / times series: $u_k \approx u(t_k)$ and $x_k \approx x(t_k)$ or $y_k \approx y(t_k)$, or





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Some methods:

 System identification (incl. ERA, N4SID, MOESP): frequency and time domain [Ho/Kalman 1966; Ljung 1987/1999; Van Overschee/De Moor 1994; Verhaegen 1994; De Wilde, Eykhoff, Moonen, Sima, ...]





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- Koopman/Dynamic Mode Decomposition (DMD): time domain [Mezič 2005; Schmid 2008; BRUNTON, KEVREKIDIS, KUTZ, ROWLEY, NOÉ, NÜSKE, SCHÜTTE, PEITZ, ...], for control systems [KAISER/KUTZ/BRUNTON 2017, B./HIMPE/MITCHELL 2018]





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- Operator inference (OpInf): time domain [Peherstorfer/Willcox 2016; KRAMER, QIAN, B., GOYAL,...]



Consider Power2Gas process for production of methane employing volatile renewable energy resources:



- High energy density
- Use of available infrastructure
- Flexible

Source: Jens Bremer (2016)



Consider Power2Gas process for production of methane employing volatile renewable energy resources:









Modeling Approach for 2D Methanation Reactor Model





Mass Balance

$$\frac{\partial \rho_{\alpha}}{\partial t} = -\frac{v_z}{\varepsilon} \frac{\partial \rho_{\alpha}}{\partial z} + \frac{\mathcal{D}_{r,i}^{\text{eff}}}{\varepsilon} \left(\frac{\partial^2 \rho_{\alpha}}{\partial r^2} + \frac{1}{r} \frac{\partial \rho_{\alpha}}{\partial r} \right) + \frac{1-\varepsilon}{\varepsilon} \tilde{M}_{\alpha} \sum_{\beta=1}^{3} \nu_{\alpha,\beta} \, \tilde{r}_{\beta}, \quad \alpha = 1 \dots 6$$

Energy Balance

$$\frac{\partial T}{\partial t} = \frac{1}{\left(\rho c_{\mathsf{p}}\right)_{\mathsf{eff}}} \left[-\rho c_{\mathsf{p}} v_z \frac{\partial T}{\partial z} + \lambda_{\mathsf{eff},\mathsf{r}} \left(\frac{\partial^2 T}{\partial r^2} + \frac{1}{r} \frac{\partial T}{\partial r} \right) + (1-\varepsilon) \sum_{\beta=1}^3 \left(-\Delta_{\mathsf{R}} \tilde{H}_\beta \right) \tilde{r}_j \right]$$

Boundary Conditions (radial)

$$\frac{\partial \rho_{\alpha}}{\partial r} = 0, \quad \frac{\partial T}{\partial r} = 0 \quad \text{ at } r = 0 \quad \left| \begin{array}{c} \frac{\partial \rho_{\alpha}}{\partial r} = 0, \quad \frac{\partial T}{\partial r} = \frac{k_{\mathrm{w}}}{\lambda_{\mathrm{eff},\mathrm{r}}} \left(T_{\mathrm{c}} - T \right) \quad \mathrm{at } r = r_{\mathrm{T}} \end{array} \right|$$

From PDAE to ODE/DAE via Finite Volume Method (FVM)



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$$\begin{aligned} & \mathsf{ODE}/\mathsf{DAE}:\\ & \dot{\mathbf{x}}(t) = \mathbf{f}(\mathbf{x}(t), \mathbf{w}(t), \mathbf{u}(t))\\ & 0 = \mathbf{w}(t) - \mathbf{d}(\mathbf{x}(t), \mathbf{u}(t)) \end{aligned}$$

 $\mathbf{x}(t)$ - "diff. state vector" $\mathbf{w}(t)$ - "alg. state vector" $\mathbf{u}(t)$ - "control vector" \mathbf{f} - strongly nonlinear RHS



 $dim(\mathbf{x}) = 350 - 5,000$ (depending on mesh refinement)



CPU Time:



CPU Time:





| $T_{ m cool,ub}$ | = | 650 | K |
|------------------|---|-----|---|
| $T_{ m cool,lb}$ | | 400 | K |
| $T_{ m ub}$ | = | 750 | K |
| $T_{ m lb}$ | | 300 | K |



Start-Up Optimal Control Problem (OCP)

$$\begin{array}{ll} \max_{\mathbf{u}(t)} & \int_{t_0}^{t_f} X_{CO_2}(\mathbf{x}(t), \mathbf{u}(t)) \ dt \ + \ R(\mathbf{u}(t)) \ \Rightarrow \mbox{time optimal start-up} \\ {\rm s.t.} & \dot{\mathbf{x}}(t) = \mathbf{f}(\mathbf{x}(t), \mathbf{u}(t)), \quad \forall t \in [t_0 \ t_f] \ \Rightarrow \mbox{reactor model} \\ & \mathbf{x}(t_0) = \mathbf{x}_0, \\ & \mathbf{x}_{ub} \ge \mathbf{x} \ge \mathbf{x}_{lb} \ \Rightarrow \mbox{reactor temperature bounds} \\ & \mathbf{u}_{ub} \ge \mathbf{u} \ge \mathbf{u}_{lb} \ \Rightarrow \mbox{cooling at reactor jacket} \end{array}$$

 $\label{eq:simultaneous optimization approach [Biegler et al.]:} orthogonal collocation on finite elements \Rightarrow large scale NLP (> 100,000 variables)$



Reduced-order model obtained from projection $(V^T V = I)$

$$\dot{\hat{x}} = V^T f(t, V\hat{x}, u), \hat{y} = g(t, V\hat{x}, u).$$

• The quality of ROM depends on the choice of V.



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- The quality of ROM depends on the choice of V.
- A common technique for nonlinear systems is Proper Orthogonal Decomposition (POD):
 - Take computed or experimental 'snapshots' of full model:

$$[x(t_1), x(t_2), \dots, x(t_N)] := X.$$



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• Perform SVD of snapshot matrix: $X = U\Sigma W^T$.



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- Perform SVD of snapshot matrix: $X = U\Sigma W^T$.
- Then, the projection matrix is V = U(:, 1:r). (Given the snapshots, this is the optimal choice w.r.t. energy.)



• Consider the nonlinear term:

$$\hat{f} = V^T f = V^T f$$

- Still, we need computations of the nonlinear function on the full grid. ~> no sufficient reduction in computational effort.
- Therefore, we require hyper-reduction; here, Discrete Empirical Interpolation Method (DEIM) [CHATARUNTABAT/SORENSEN 2010].



• The idea is:



where

- 'T' is a rectangular matrix, and
- the vector 'c' contains the nonlinear function evaluations at specific grid points.









• Use greedy algorithm to select the important grid points (DEIM points) for approximating the nonlinear function via interpolation.



Original system (full-order model, FOM):

$$\begin{aligned} & \overset{\text{ODE:}}{\mathbf{x} = \mathbf{f}(\mathbf{x}, \mathbf{u})} \\ & & \downarrow \\ \\ & \mathbf{\dot{x}} = \mathbf{A}_{1}(\mathbf{x}) \mathbf{x} + \mathbf{A}_{2} \mathbf{x} + \mathbf{B}_{1}(\mathbf{x}) \mathbf{u}_{1} + \mathbf{B}_{2} \mathbf{u}_{2} + \mathbf{f}(\mathbf{x}) \\ & \stackrel{\uparrow}{\mathbf{D}_{r,\alpha}} \stackrel{\uparrow}{\mathbf{h}_{\alpha}} & \stackrel{\uparrow}{\mathbf{h}_{\alpha}} \stackrel{\bullet}{\mathbf{h}_{\alpha}} \stackrel{$$



• POD-DEIM leads to the the following system:

$$\begin{split} \dot{\mathbf{x}}_r &= \mathbf{Q}_A \mathbf{P}_A \mathbf{A}_1(\mathbf{x}^*) \, \mathbf{x}^* + \mathbf{V}^T \mathbf{A}_2 \, \mathbf{V} \mathbf{x}_r + \mathbf{Q}_B \mathbf{P}_B \mathbf{B}_1(\mathbf{x}^*) \, \mathbf{u}_1 + \mathbf{V}^T \mathbf{B}_2 \, \mathbf{u}_2 + \mathbf{Q}_f \mathbf{P}_f \mathbf{f}(\mathbf{x}^*), \\ \mathbf{y} &= \mathbf{L}^T \, \mathbf{x}^*, \\ \text{where } \mathbf{x}^* &= \mathbf{V} \mathbf{x}_r, \qquad \text{with } \dim(\mathbf{x}_r) \ll \dim(\mathbf{x}). \end{split}$$

- V from SVD of x snapshots (POD)
- \mathbf{Q}_A from SVD of $\mathbf{A}_1(\mathbf{x}) \mathbf{x}$ snapshots (DEIM)
- \mathbf{Q}_B from SVD of $\mathbf{B}_1(\mathbf{x}) \mathbf{x}$ snapshots (DEIM)
- \mathbf{Q}_f from SVD of $\mathbf{f}(\mathbf{x})$ snapshots (DEIM)

e.g., for
$$\mathbf{f}(\mathbf{x})$$

$$SVD \begin{bmatrix} \frac{f_1(\mathbf{x}(t_1)) & f_1(\mathbf{x}(t_2)) & f_1(\mathbf{x}(t_3)) & \cdots}{f_2(\mathbf{x}(t_1)) & f_1(\mathbf{x}(t_2)) & f_3(\mathbf{x}(t_3)) & \cdots} \\ \frac{f_3(\mathbf{x}(t_1)) & f_1(\mathbf{x}(t_2)) & f_1(\mathbf{x}(t_3)) & \cdots}{\vdots & \vdots & \vdots & \ddots} \end{bmatrix}$$



Scenario 1: start-up phase



Scenario 2: continuous operation



- The range of $x_{CO2} \in [0.7, 0.9]$.
- The range of $x_{H2} \in [0.1, 0.3]$.
- The range of $T_{cool} \in [500K, 700K]$.

- No. Training cases: 50
- No. Test cases: 20







































| model | no. | avg. | median of $arepsilon$ / % | | | | | | |
|--------|--------|----------|------------------------------------|-----------------------------------|------------------------------------|------------------------------------|-----------------------------------|-----------------------------------|----------------------------------|
| | states | CPU-time | $\bar{\varepsilon}_{\mathrm{CH4}}$ | $\bar{\varepsilon}_{\mathrm{CO}}$ | $\bar{\varepsilon}_{\mathrm{CO2}}$ | $\bar{\varepsilon}_{\mathrm{H2O}}$ | $\bar{\varepsilon}_{\mathrm{H2}}$ | $\bar{\varepsilon}_{\mathrm{N2}}$ | $\bar{\varepsilon}_{\mathrm{T}}$ |
| FOM-S1 | 4375 | 19.5 s | - | - | - | - | - | - | - |
| ROM-S1 | 34 | 1.3 s | 1.16 | 2.06 | 0.84 | 1.12 | 0.88 | 0.22 | 0.02 |
| FOM-S2 | 4375 | 39.8 s | - | - | - | - | - | - | - |
| ROM-S2 | 36 | 2.4 s | 1.77 | 3.27 | 1.13 | 1.74 | 1.29 | 0.56 | 0.18 |



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- Updating the surrogate models using current measurements/data of a chemical process requires the fusion of model order reduction with data assimilation techniques!
- Smart process engineering will require digital twins, building on
 - the accuracy of high-fidelity models inherited by the surrogates obtained from model order reduction;
 - calibration of the surrogate models using measurement data;
 - efficient data assimilation techniques for updating the surrogates.





Selected References



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Commercial 1: 3-Volume Handbook "Model Order Reduction"



- Edited by Peter Benner, Stefano Grivet-Talocia, Alfio Quarteroni, Gianluigi Rozza, Wil Schilders, and Luís Miguel Silveira,
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- published by DeGruyter in 2021, ebook is fully Open Access!



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