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FOR DYNAMICS OF COMPLEX
TECHNICAL SYSTEMS
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COMPUTATIONAL METHODS IN
SYSTEMS AND CONTROL THEORY

Infering Discrete and Reduced Fluid-Structure Interaction Models from Data

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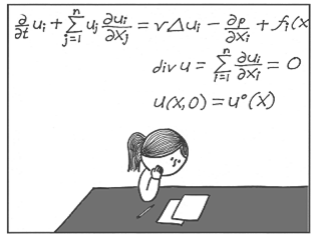
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Overview



- **Adjacency-based non-intrusive modelling**
 - Inference of Numerical Schemes
 - Motivating example: 2D Burgers' equation



- **Application to incompressible Navier Stokes**
 - Inference of sparse FOM / POD
 - Numerical Aspects (centering / regularization)
 - sFOM-POD / OpInf comparison (cylinder flow)



- **Fluid-Structure Interactions (FSI)**
 - Governing Equations
 - Laminar Vortex-Induced Vibrations (VIV)
 - Hron-Turek Benchmark FSI3



Inference of Numerical Schemes



- We look at PDEs of the form: $\frac{\partial u}{\partial t} = \mathcal{P}(u, u_x, u_{xx}, u_y, u_{yy}, u_{xy}..)$, where $\mathcal{P}(\cdot)$ is a polynomial operator.

- Discretizing the right hand side in space, we obtain a system of ODEs for each spatial point \vec{x}_i :

$$\left. \frac{du}{dt} \right|_{\vec{x}_i} = \sum_{j \in q_i} f_j \beta_j = \mathbf{f}_{q_i}^T \boldsymbol{\beta}_i$$

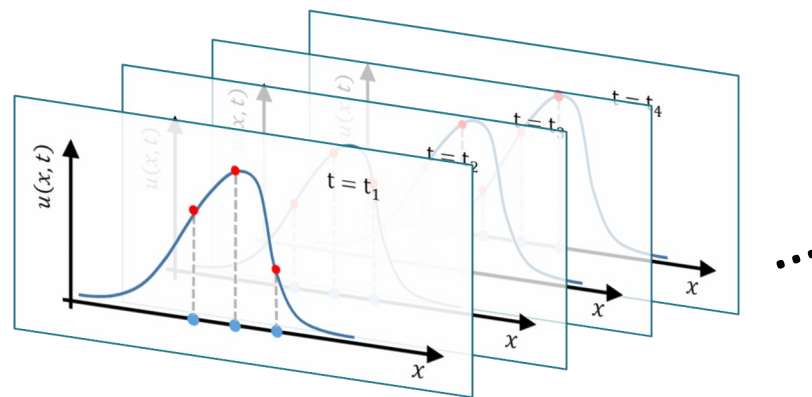
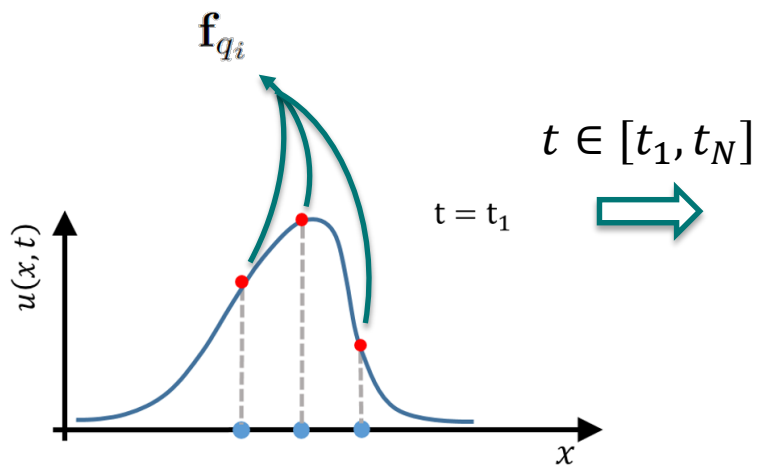


e.g. for a 1D linear system (*heat eq.*) and a 3-pt symmetric stencil:

$$\mathbf{f}_{q_i} = [u_{i-1}, u_i, u_{i+1}]^T$$

and $\boldsymbol{\beta}_i$ are corresponding coefficients.

Numerical Scheme Inference: Can we infer $\boldsymbol{\beta}_i$, given data over $t \in [t_1, t_N]$ for $\left. \frac{du}{dt} \right|_{\vec{x}_i}$ and \mathbf{f}_{q_i} ?



Least squares formulation:

$$\min_{\boldsymbol{\beta}_i} \|\mathcal{D}_i \boldsymbol{\beta}_i - \mathbf{d}_i\|_2$$

with: $\mathcal{D}_i = \begin{bmatrix} \mathbf{f}_{q_i}^T(t_1) \\ \vdots \\ \mathbf{f}_{q_i}^T(t_N) \end{bmatrix}$, $\mathbf{d}_i = \begin{bmatrix} \left. \frac{du}{dt} \right|_{(i,t_1)} \\ \vdots \\ \left. \frac{du}{dt} \right|_{(i,t_N)} \end{bmatrix}$

Baddoo et al. (2021), Schumann Y., & Neumann P. (2022)



A nonlinear example: 2D Burgers' equation

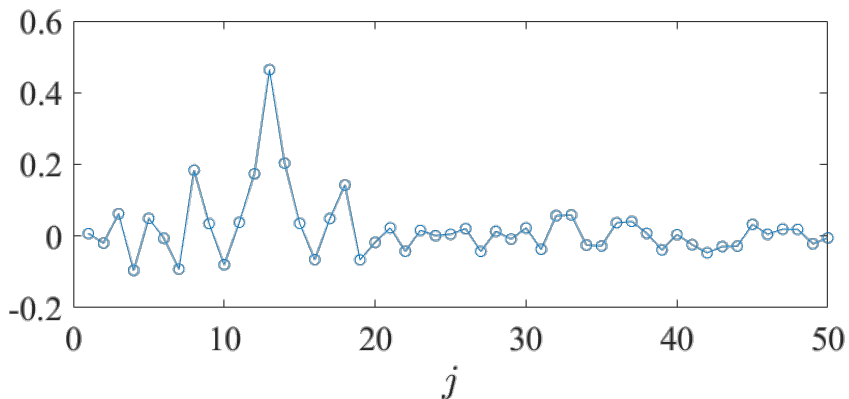
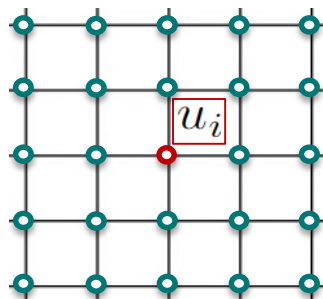


$$\frac{\partial u}{\partial t} = cu \nabla \cdot u + \nu \nabla^2 u$$

Periodic BCs for $(x, y) \in [0, 1] \times [0, 1]$

$$u(t = 0) = \cos(2\pi x)\cos(2\pi y)$$

Numerical stencil:



Discretizing in space and time, we get:

$$\mathbf{u}_{n+1} = A\mathbf{u}_n + Q\mathbf{u}_n \circ \mathbf{u}_n$$

where A and Q are sparse matrices.

We aim to infer the entries of A, Q .
These correspond to vector β_α

$$\min_{\beta_\alpha} \|\mathcal{D}_\alpha \beta_\alpha - \mathbf{d}_\alpha\|_2$$

- We collect data for $\nu = 2 \times 10^{-3}, c = 0.2, \Delta x = \Delta y = 0.02, \Delta t = 0.01$, using a **second-order scheme in space**.

- Regularization is necessary: We truncate the SVD of \mathcal{D}_α , which is equivalent to an L_2 regularization:

$$\min_{\beta_\alpha} \|\mathcal{D}_\alpha \beta_\alpha - \mathbf{d}_\alpha\|_2^2 + \lambda \|\beta_\alpha\|_2^2$$

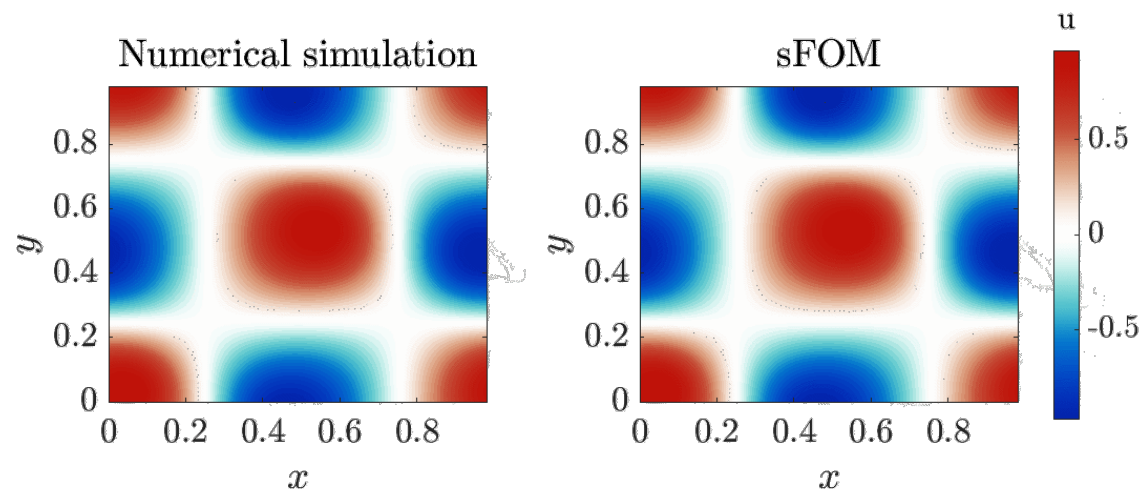
- Observation: A strict truncation limit of $\sigma / \max(\sigma) = 10^{-4}$ is needed: Potentially **linked to the order of the scheme** used for simulation.



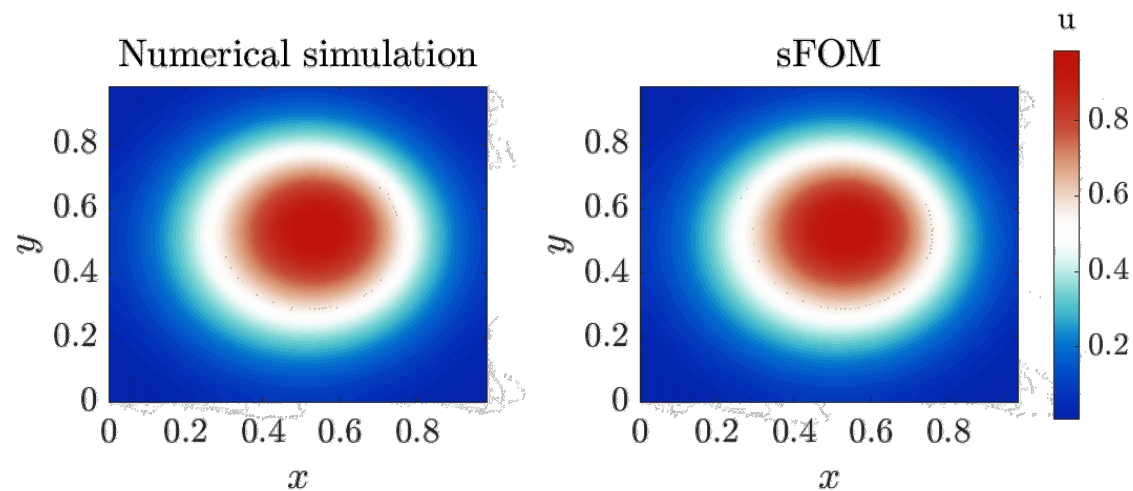
A nonlinear example: 2D Burgers'



Simulation results:

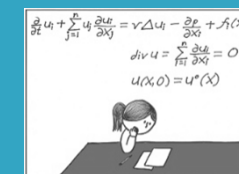


We simulate the inferred system with different initial conditions: $u(t = 0) = e^{-10(x-0.5)^2} e^{-10(y-0.5)^2}$





Sparse FOM for incompressible N-S



Incompressible N-S:

$$\begin{cases} \nabla \cdot \mathbf{u} = 0 \\ \frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} = \frac{1}{\rho_f} \nabla \cdot \boldsymbol{\sigma} + \mathbf{f} \end{cases}$$

$$\text{Discretizing in space: } \begin{cases} \frac{\partial \mathbf{u}}{\partial t} = A_1 \mathbf{u} + A_2 \mathbf{p} + H \mathbf{u} \otimes \mathbf{u} \\ A_2^T \mathbf{u} = \mathbf{0} \end{cases}$$

where: $A_1 \in \mathcal{R}^{n_u \times n_u}$, $A_2 \in \mathcal{R}^{n_u \times n_p}$, $H \in \mathcal{R}^{n_u \times n_u^2}$

In projection-based methods:

$$\tilde{\mathbf{u}} = U^T \mathbf{u}$$

where $U \in \mathcal{R}^{n_u \times r}$
and $r \ll n_u$

...after cancelling out pressure:

$$\mathbf{u}^{k+1} = \mathbf{A} \mathbf{u}^k + \mathbf{H} \mathbf{u}^k \otimes \mathbf{u}^k + \mathbf{K} \mathbf{u}_{in} + \mathbf{C}$$

P.B. et al. (2021)

with adjacency-based, sparse \mathbf{A} , \mathbf{H} , \mathbf{K}

We can use the local inference of numerical schemes, scaling with n_u

Pros:

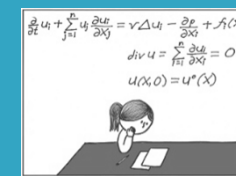
- (+) Direct enforcement of Dirichlet BCs (e.g. \mathbf{K} known a priori).
- (+) FOM independence from projection basis.

Cons:

- (-) $\uparrow\uparrow$ in offline computational cost.
- (-) Need for adjacency information (mesh construction).

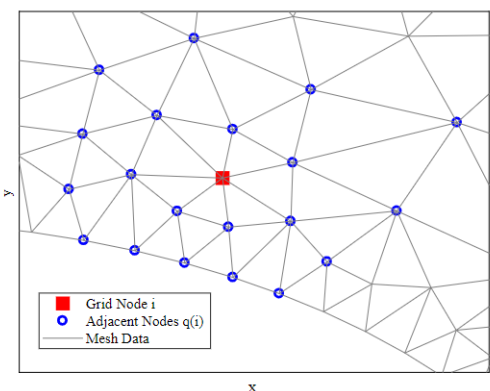


Sparse FOM inference - POD



1st step: Interpolate data $\forall t$ to a grid (or construct adjacency matrix of an existing grid).

2nd step: To enforce adjacency-based sparsity, we examine each DOF i independently:



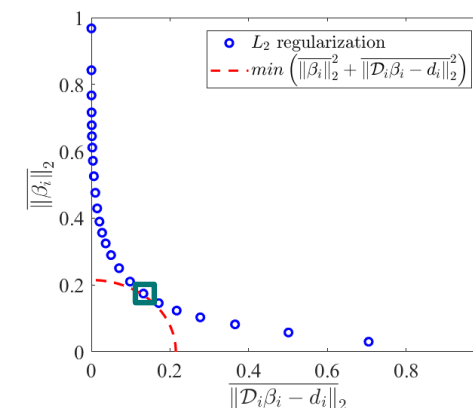
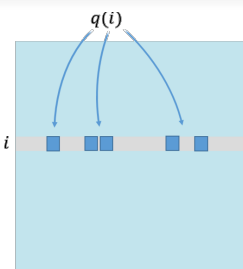
adj. info +
data for $t \in [t_1, t_N]$

Least-Squares formulation

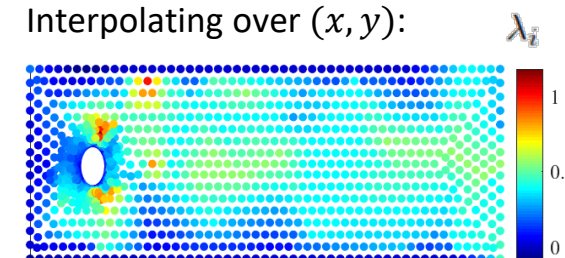
$$\min_{\beta_i} \|\mathcal{D}_i \beta_i - \mathbf{d}_i\|_2^2 + \lambda_i \|\beta_i\|_2^2$$

where:

$$\mathcal{D}_i = \begin{bmatrix} \mathbf{f}_{q_i}^T(t_1) \\ \vdots \\ \mathbf{f}_{q_i}^T(t_N) \end{bmatrix}, \quad \mathbf{d}_i = \begin{bmatrix} \left. \frac{du}{dt} \right|_{(i,t_1)} \\ \vdots \\ \left. \frac{du}{dt} \right|_{(i,t_N)} \end{bmatrix}$$



Interpolating over (x, y) :



3rd step: Store the values of β_i to the FOM sparse matrices.

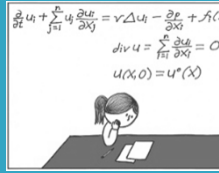
4th step: Project to ROM through Proper Orthogonal Decomposition (POD).

“smart” projection due to **known** sparsity

e.g: $\tilde{A} = U^T A U$ $\tilde{H} = U^T H U \otimes U$



Cylinder flow results

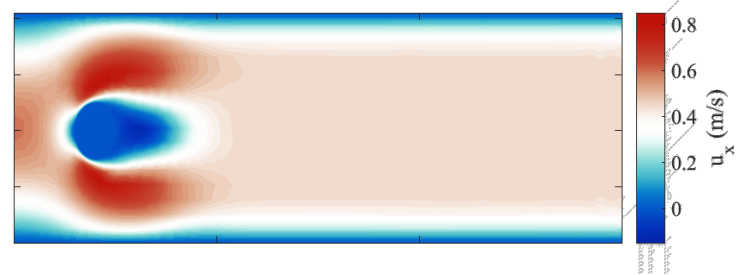


We examine this formulation for a laminar, incompressible flow over a cylinder:

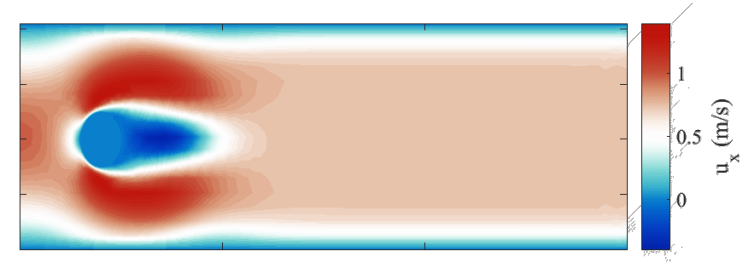
- 65% training time for ROMs (over which system operators are inferred, also for OpInf (Peherstorfer, & Willcox (2016))).

- Average error over the domain:
$$e(t) = \frac{\|\mathbf{u}_{x_{CFD}} - \mathbf{u}_{x_{ROM}}\|_1}{n \max(\mathbf{u}_{x_{CFD}} - \bar{\mathbf{u}}_{x_{CFD}})} \times 100\%$$

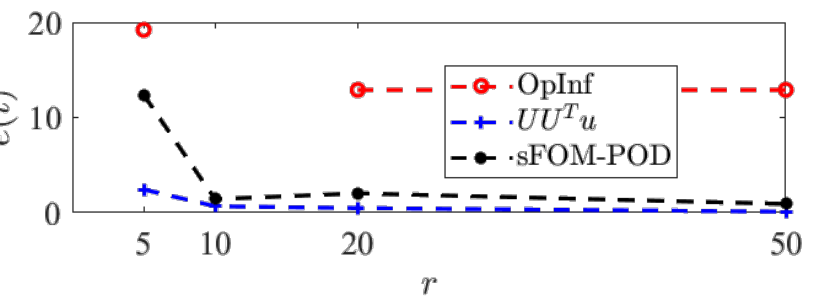
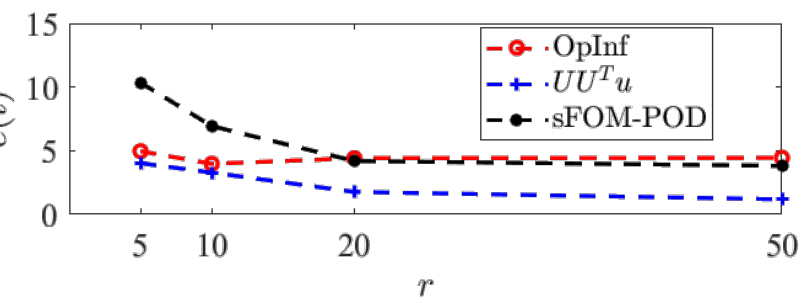
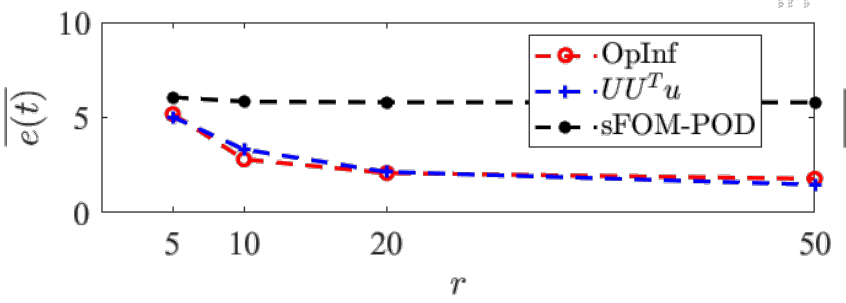
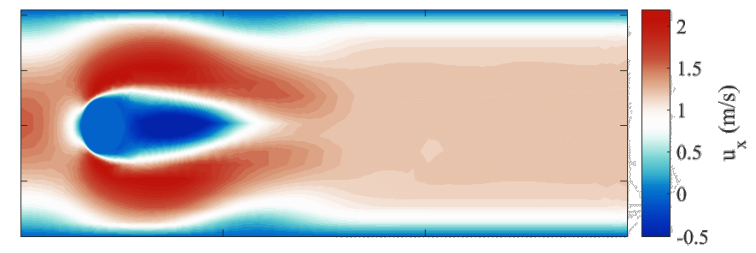
$Re = 60$



$Re = 100$



$Re = 160$



Computational (clock) offline time:
 OpInf $O(t_{OpInf}) = 1 s$, sFOM $O(t_{sFOM}) = 60 s$



Numerical simulations performed with Gascoigne3D (open-source, finite element solver)



Fluid-Structure Interactions (FSI)



Incompressible N-S equations (Arbitrary Lagrangian-Eulerian formulation):

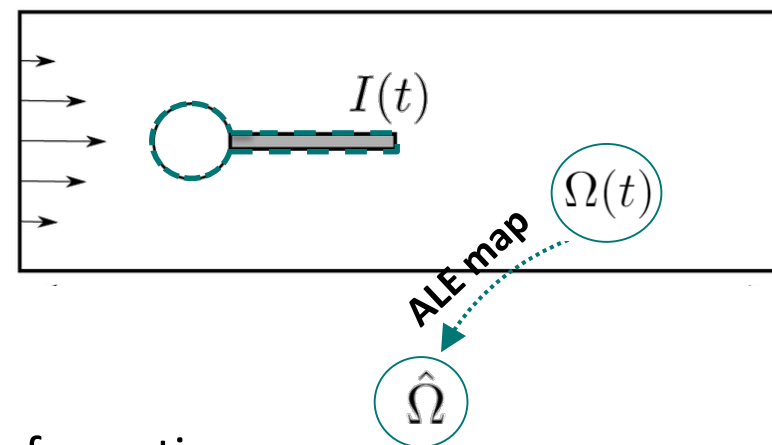
$$\begin{cases} \rho_f \left(\partial_t \hat{\mathbf{u}} + \hat{\nabla} \hat{\mathbf{u}} \cdot I \left(\hat{\mathbf{u}} - \partial_t \hat{\mathbf{d}} \right) \right) - \\ - \operatorname{div} \left(\hat{\sigma}(\hat{\mathbf{u}}, \hat{p}) \right) = \rho_f \vec{g} \\ \operatorname{div} \left(I \hat{\mathbf{u}} \right) = 0 \end{cases}$$

Solid Navier-Lamé equations:

$$\begin{cases} \partial_{tt} \mathbf{d}_s - \nabla \cdot \boldsymbol{\sigma}_s = 0 \\ \boldsymbol{\sigma}_s = \mu(\nabla \mathbf{d}_s + \nabla \mathbf{d}_s^T) + \lambda \operatorname{tr}(\frac{1}{2}(\nabla \mathbf{d}_s + \nabla \mathbf{d}_s^T)) I \end{cases}$$

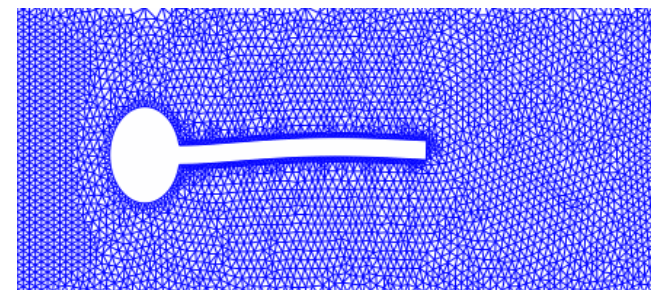
Coupling conditions:

$$\begin{cases} \mathbf{n}_f \cdot \boldsymbol{\sigma}_f = -\mathbf{n}_s \cdot \boldsymbol{\sigma}_s \text{ on } I(t) \\ \partial_t \mathbf{d}_s = \mathbf{u}_f \text{ on } I(t) \end{cases}$$



Grid deformation:

$$\begin{cases} -\nabla^2 \hat{\mathbf{d}}_f - \frac{\nabla_a}{a} \nabla \hat{\mathbf{d}}_f = \mathbf{0}, & \text{in } \hat{\Omega} \times (0, T] \\ \hat{\mathbf{d}}_f = \hat{\mathbf{d}}_s - \hat{\mathbf{d}}_s(t=0), & \text{on } I(t) \\ \hat{\mathbf{d}}_f = \mathbf{0}, & \text{on external boundaries} \end{cases}$$





VIV: Coupled sFOM-POD/ First-principle models

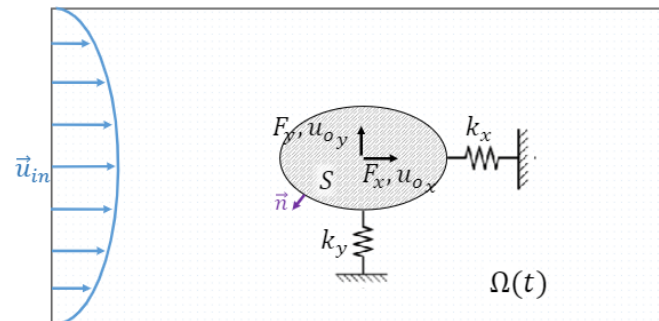


Non-deformable solid dynamics (4 DOFs):

$$\rho_s A_s \partial_{tt} \mathbf{d}_s + K \mathbf{d}_s = (\rho_s - \rho_f) A_s \vec{g} + \int_{\partial S} \sigma(\mathbf{u}, p) \vec{n} ds$$

Quadratic-bilinear data-driven model for the fluid part:

$$\mathbf{u}_F^k = A \mathbf{u}_F^{k-1} + H \mathbf{u}_F^k \otimes \mathbf{u}_F^k + K \partial_t \mathbf{d}_s^k \otimes \mathbf{u}_F^k + B \partial_t \mathbf{d}_s^k + L \mathbf{u}_{in}^k + C_F$$



Performing POD, we obtain the coupled Fluid/Structure ROM:

Fluid part (**data-driven**)

Solid part (**physics**)

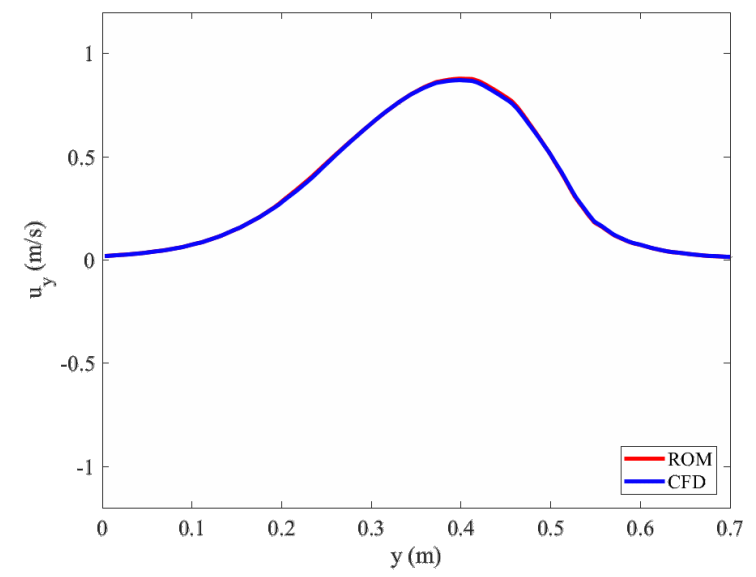
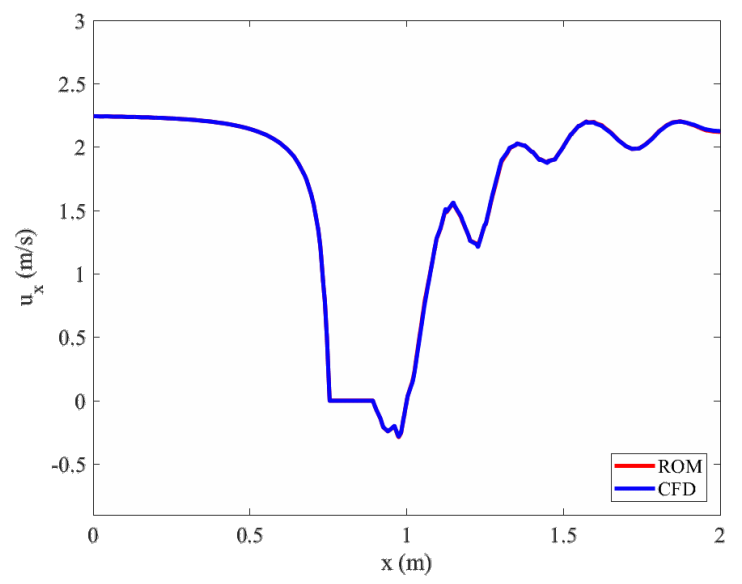
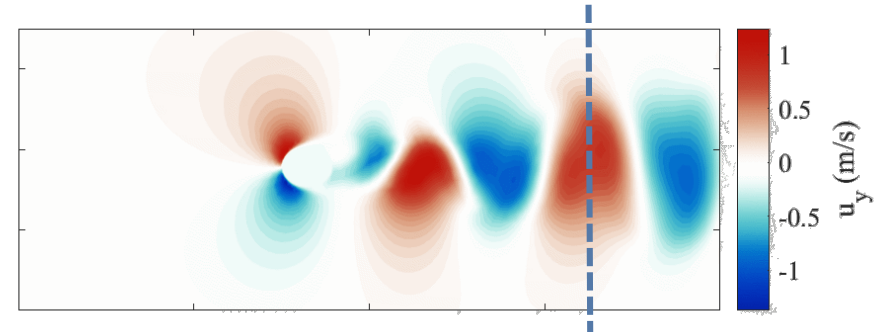
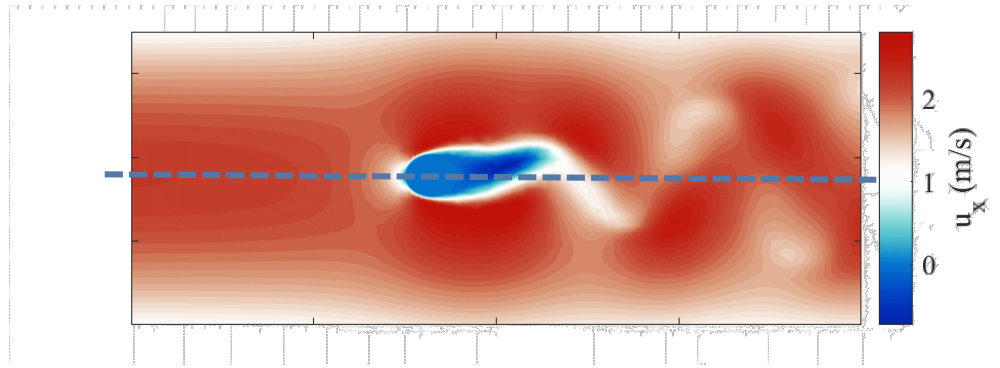
$$\left\{ \begin{array}{l} \tilde{\mathbf{u}}^k = \tilde{A} \tilde{\mathbf{u}}^{k-1} + \tilde{H} \tilde{\mathbf{u}}^k \otimes \tilde{\mathbf{u}}^k + \tilde{K} \partial_t \mathbf{d}_s^k \otimes \tilde{\mathbf{u}}^k + \\ \quad + \tilde{B} \partial_t \mathbf{d}_s^k + \tilde{L} \mathbf{u}_{in} + \tilde{C} \\ \mathbf{F}^k = \tilde{A}_F \tilde{\mathbf{u}}^k + \tilde{H}_F \tilde{\mathbf{u}}^k \otimes \tilde{\mathbf{u}}^k \end{array} \right. \left\{ \begin{array}{l} \partial_t \mathbf{d}_s^k + \frac{\Delta t K}{2 \rho_s A_s} \mathbf{d}_s^k - \frac{\Delta t}{2} \mathbf{F}^k \\ = \partial_t \mathbf{d}_s^{k-1} - \frac{\Delta t K}{2 \rho_s A_s} \mathbf{d}_s^{k-1} + \Delta t \mathbf{g} + \frac{\Delta t}{2} \mathbf{F}^{k-1} \\ \mathbf{d}_s^k - \frac{\Delta t}{2} \partial_t \mathbf{d}_s^k \\ = \mathbf{d}_s^{k-1} + \frac{\Delta t}{2} \partial_t \mathbf{d}_s^{k-1} \end{array} \right.$$



Results for $Re = 180$



ROM with 20 DOFs built for CFD data $t < 3.80$ s, predictions for $t = 3.80 \rightarrow 5.91$ s



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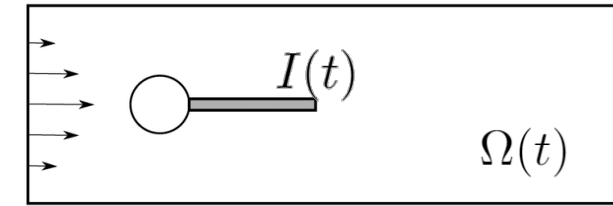
FSI: Coupled data-driven models



Fluid model:

$$\mathbf{u}_F^k = A_F \mathbf{u}_F^{k-1} + H_F \mathbf{u}_F^k \otimes \mathbf{u}_F^k + K_F \underline{\partial_t \mathbf{d}_F^k} \otimes \mathbf{u}_F^k + B_F \partial_t \mathbf{d}_s^k + L_F \mathbf{u}_{in}^k + C_F$$

Computed from Laplace equation: $\partial_t \mathbf{d}_F^k = A_L \partial_t \mathbf{d}_s^k$



Deformable solid model:

2nd order oscillatory system: $\partial_t \mathbf{d}_s^k = A_S \underline{\partial_t \mathbf{d}_s^{k-1}} + K_S \underline{\mathbf{d}_s^{k-1}} + \mathbf{f}$

Forcing from the fluid stress tensor normal: $\mathbf{f} = B_S \mathbf{u}_{FS}^k + H_S \mathbf{u}_{FS}^k \otimes \mathbf{u}_{FS}^k$

Crank-Nicholson scheme for displacement update: $\mathbf{d}_s^k = \mathbf{d}_s^{k-1} + \frac{\Delta t}{2} (\partial_t \mathbf{d}_s^k + \partial_t \mathbf{d}_s^{k-1})$

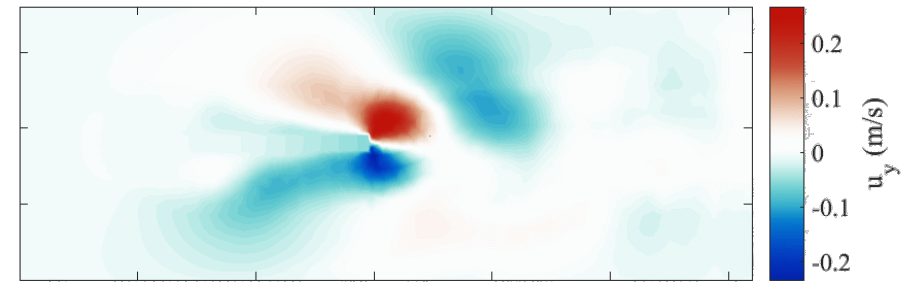
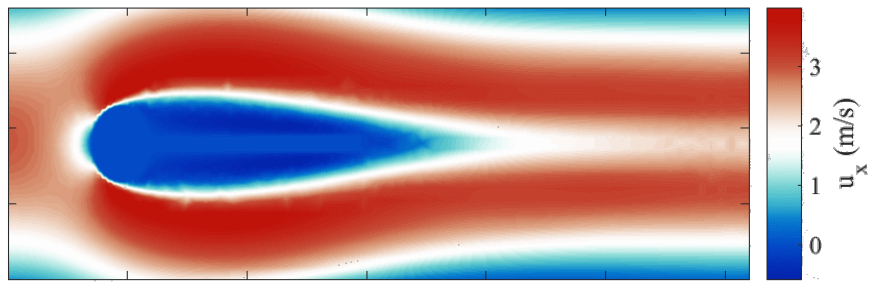


Hron-Turek Benchmark FSI3

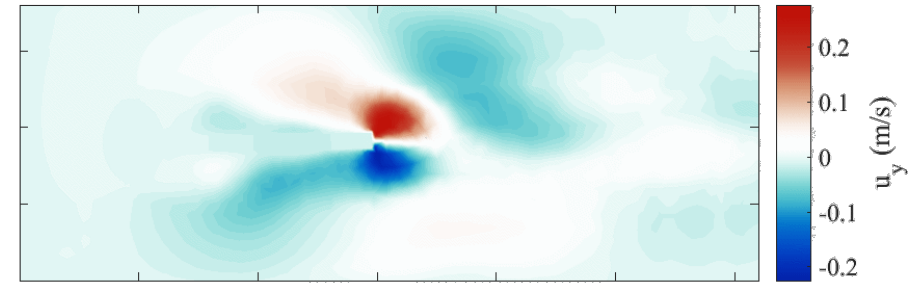
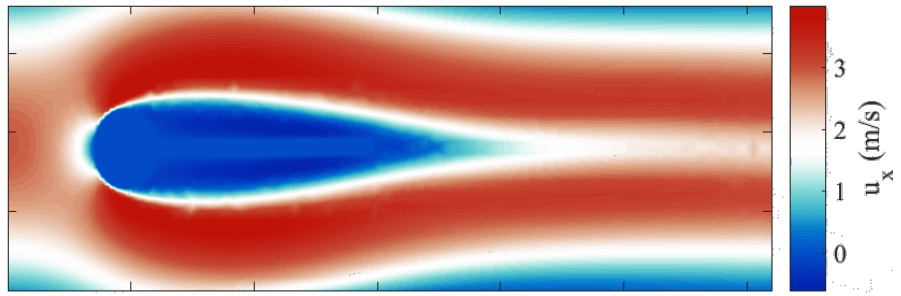


We examine the benchmark at $Re = 200$, with $t_{train} = 1.92 s$, $t_{tot} = 3.06 s$:

CFD data ($n = 4128$):



sFOM-POD ($r_F = 20, r_S = 5$):



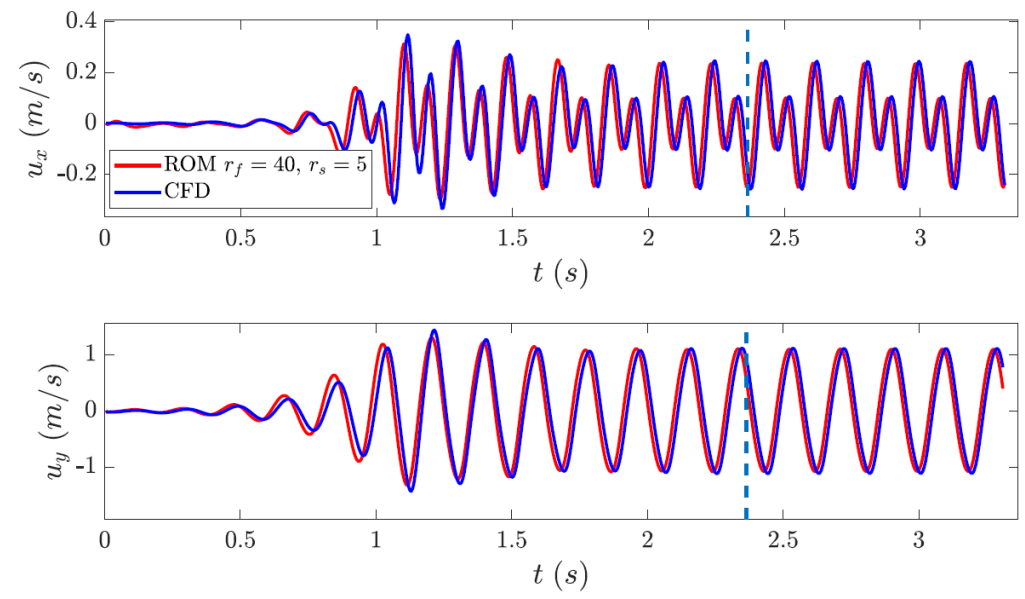
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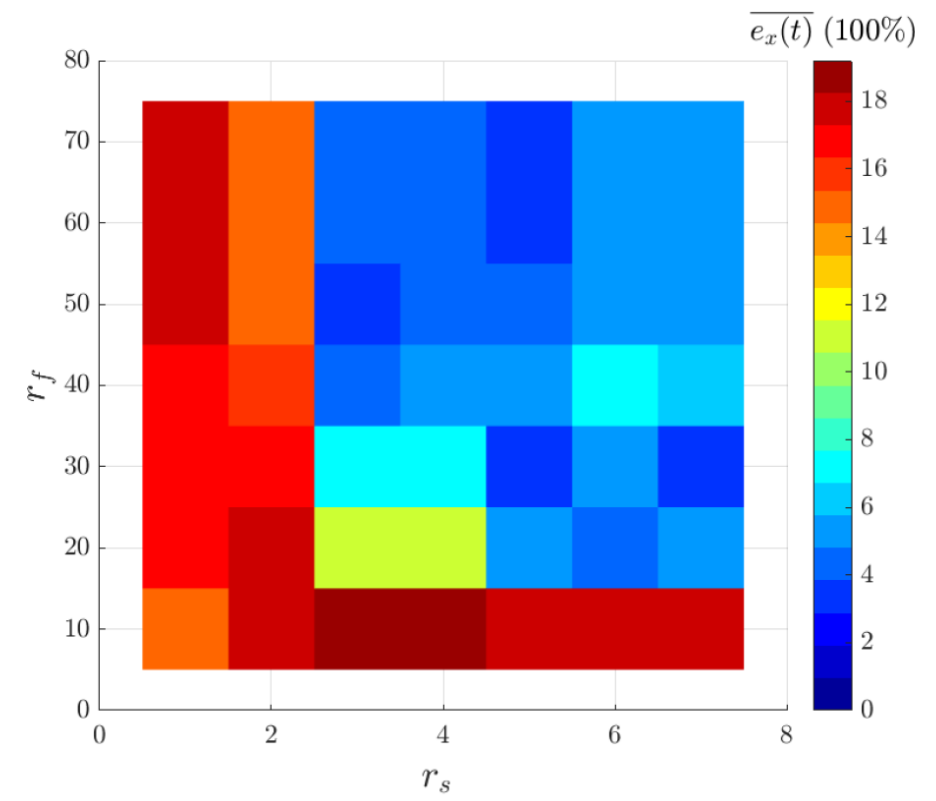
Hron-Turek Benchmark FSI3



Velocity at the tip of the solid tail:



Prediction error w.r.t the POD basis dimensions r_f, r_s



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Conclusion / Future Work

So Far:

- ✓ Developed an **adjacency-based** method for **sparse, non-intrusive** modelling.
- ✓ Showcased model accuracy for 3 cases: **Flow over cylinder, 2D VIV, 2D FSI**.
- ✓ Investigated **method properties** compared to other intrusive and non-intrusive approaches.

Current / Future Work:

- Consideration of local **physical constraints** (e.g. energy preservation) for inferred schemes.
- **Theoretical investigation** of numerical scheme inference properties.
- **Domain decomposition** and **parallelization** of LS problems.
- Extension to **parametric ROMs** (VIV, FSI applications).



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