

Riccati-Based Boundary Feedback Stabilization of Multi-Field Flow Problems

We present recent progress in the numerical realization for boundary feedback stabilization for Navier-Stokes equations. Therefor, we will explain how the projection idea of [HEINKENSCHLOSS/SORENSEN/SUN '05] can be used to apply the approach of Raymond [RAYMOND '06] for boundary feedback stabilization of (Navier-)Stokes equations. To this end, we will illustrate details about the arising nested iteration and how we treat the connected technical difficulties.

Furthermore, we will introduce a more complicated application, namely the boundary feedback stabilization of a coupled system of Navier-Stokes equations and a diffusion-convection equation that describes the spread of a concentration within the flow field. We will point out the system structure and the analogies to the pure Navier-Stokes system.

Riccati-Based Boundary Feedback Stabilization of Multi-Field Flow Problems

Eberhard Bänsch¹ Peter Benner^{2,3} Jens Saak^{2,3} Martin Stoll²
Heiko K. Weichelt³ Stephan Weller¹

¹ Friedrich-Alexander-Universität Erlangen-Nürnberg
Department of Applied Mathematics III

² Max Planck Institute for Dynamics of Complex Technical Systems Magdeburg,
Research group Computational Methods in Systems and Control Theory

³ Chemnitz University of Technology, Department of Mathematics,
Research group Mathematics in Industry and Technology



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Overview

- 1 Problem Setting
- 2 Workflow
- 3 Numerical Examples
- 4 Conclusion

Problem Setting

Test-Scenarios: NSE on von Kármán Vortex Street

PDE: NSE

Goal: $\vec{z} = \vec{v} - \vec{w} \rightarrow 0$

↔ Linearized Navier-Stokes equations:

$$\frac{\partial \vec{z}}{\partial t} - \frac{1}{\text{Re}} \Delta \vec{z} + (\vec{z} \cdot \nabla) \vec{w} + (\vec{w} \cdot \nabla) \vec{z} + \nabla p = 0$$

$$\text{div } \vec{z} = 0$$

defined for $t \in (0, \infty)$ and $\vec{x} \in \Omega$
+ boundary and initial conditions

LQR

Minimize

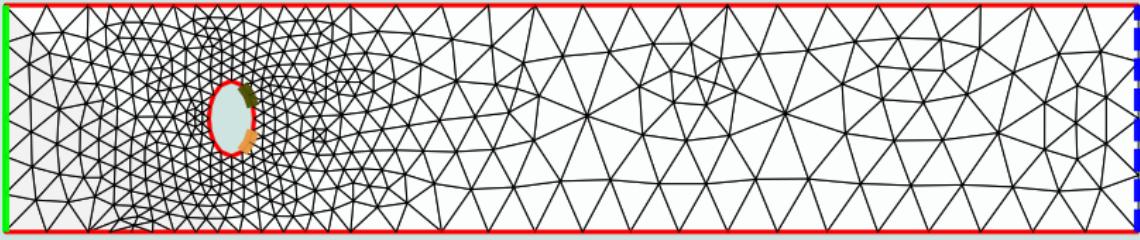
$$\mathcal{J}(\mathbf{y}, \mathbf{u}) = \frac{1}{2} \int_0^\infty \lambda \|\mathbf{y}\|^2 + \frac{1}{\rho} \|\mathbf{u}\|^2 dt$$

s.t.

$$\begin{bmatrix} M & 0 \\ 0 & 0 \end{bmatrix} \frac{d}{dt} \begin{bmatrix} \mathbf{z} \\ \mathbf{p} \end{bmatrix} = \begin{bmatrix} A & G \\ G^T & 0 \end{bmatrix} \begin{bmatrix} \mathbf{z} \\ \mathbf{p} \end{bmatrix} + \begin{bmatrix} B \\ 0 \end{bmatrix} \mathbf{u}$$

$$\mathbf{y}(t) = C\mathbf{z}(t)$$

Domain Ω : von Kármán vortex street



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NSE

stationary NSE

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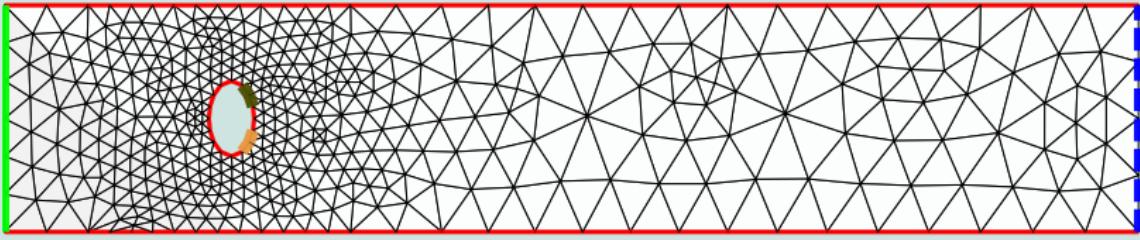
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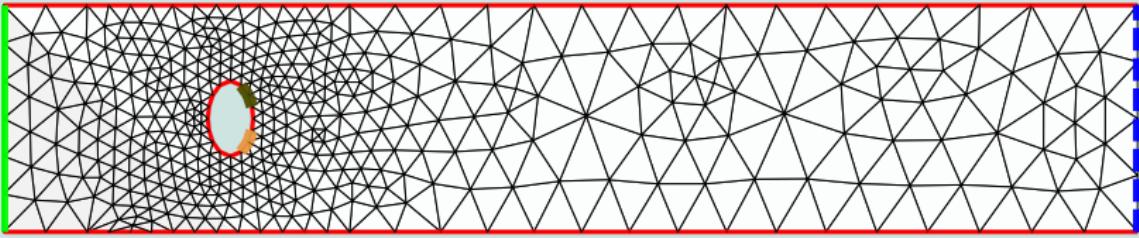
s.t.

$$\mathcal{M} \frac{d}{dt} \tilde{\mathbf{z}} = \mathcal{A} \tilde{\mathbf{z}} + \mathcal{B} \mathbf{u}$$

$$\mathbf{y}(t) = \mathcal{C} \tilde{\mathbf{z}}$$

[HEINKENSCHLOSS/SORENSEN/SUN '08]

Domain Ω : von Kármán vortex street



Problem Setting

Test-Scenarios: NSE Coupled with DCE in Reactor Model

PDE: NSE+DCE

Goal: $\vec{z} = \vec{v} - \vec{w} \rightarrow 0, c = c^{(\vec{v})} - c^{(\vec{w})} \rightarrow 0$

~~ Linearized coupled system:

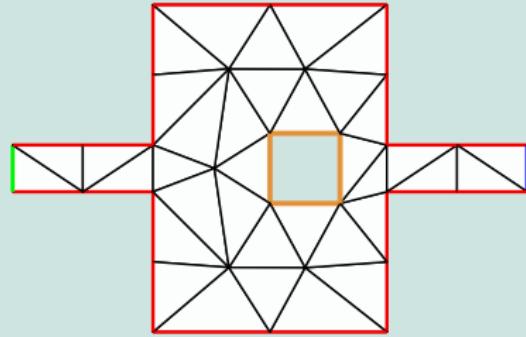
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$$\frac{\partial c}{\partial t} - \frac{1}{\text{Re Sc}} \Delta c + (\vec{w} \cdot \nabla) c + (\vec{z} \cdot \nabla) c^{(\vec{w})} = 0$$

$$\operatorname{div} \vec{z} = 0$$

defined for $t \in (0, \infty)$, $\vec{x} \in \Omega$ and some BC,IC

Domain Ω : Reactor Model



LQR

Minimize

$$\mathcal{J}(\mathbf{y}, \mathbf{u}) = \frac{1}{2} \int_0^{\infty} \lambda \|\mathbf{y}\|^2 + \frac{1}{\rho} \|\mathbf{u}\|^2 dt$$

s.t.

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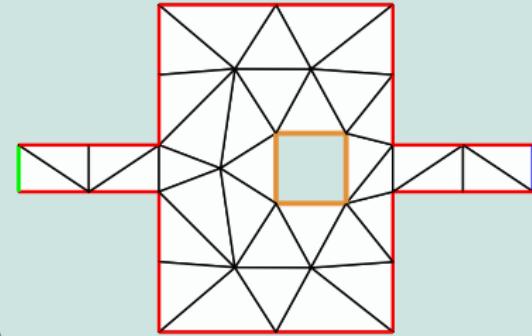
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stationary DCE in Ω : Reactor Model



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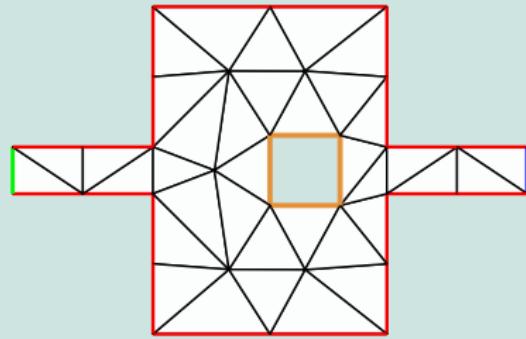
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[HEINKENSCHLOSS/SORENSEN/SUN '08]



Workflow

LQR for Nonlinear PDEs with Algebraic Constraints

Continuous Level

- Linearize around a given stationary trajectory.
- Index reduction via projection method. [HEINKENSCHLOSS/SORENSEN/SUN '08]
- Formulate stabilization problem for the perturbation.



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Semi-Discretized Level

- Discretization via inf-sup stable FE (Taylor-Hood-Elements).
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- Find feedback matrix \mathcal{K} depending on cost functional and projected ODE.

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- Apply feedback \mathcal{K} within NAVIER.
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Workflow

Leray Projection

Continuous Level

$$P : (L^2(\mathbb{R}^d)^d) \rightarrow \mathbf{H}_{\text{div } 0}(\mathbb{R}^d)$$

To compute \vec{v}_{div} , solve for given \vec{v}

$$\vec{v}_{\text{div}} + \nabla p = \vec{v},$$

$$\operatorname{div} \vec{v}_{\text{div}} = 0.$$

Semi-Discretized Level

OCIP 2012

[HEINKENSCHLOSS/SORENSEN/SUN '08]

Index reduction idea for

Lyapunov-solver:

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$$\mathbf{p} = (G^T M^{-1}G)^{-1}G^T \mathbf{v}$$

$$M\mathbf{w} = M(I - M^{-1}G(G^T M^{-1}G)^{-1}G^T)\mathbf{v}$$

Workflow

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$$\begin{aligned} \mathbf{p} &= (G^T M^{-1}G)^{-1}G^T \mathbf{v} \\ \mathbf{w} &= (I - M^{-1}G(G^T M^{-1}G)^{-1}G^T)\mathbf{v} \end{aligned}$$

Leray vs. Π^T

$$\vec{w} = P(\vec{v}) \Rightarrow \mathbf{w} = \Pi^T \mathbf{v}$$

$$0 = \operatorname{div} \vec{w} \Rightarrow 0 = G^T \mathbf{w}$$



Workflow

Nested Iteration

Compute feedback matrix $\mathcal{K} = \mathcal{B}^T X \mathcal{M}$ with X solves:

$$\mathcal{R}(X) = \mathcal{C}^T \mathcal{C} + \mathcal{A}^T X \mathcal{M} + \mathcal{M}^T X \mathcal{A} - \mathcal{M}^T X \mathcal{B} \mathcal{B}^T X \mathcal{M} = 0$$

Newton Kleinman method



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Step $m+1$: solve Lyapunov equation

$$(\mathcal{A} - \mathcal{B} \mathcal{K}^{(m)})^T X^{(m+1)} \mathcal{M} + \mathcal{M}^T X^{(m+1)} (\mathcal{A} - \mathcal{B} \mathcal{K}^{(m)}) = -(\mathcal{W}^{(m)})^T \mathcal{W}^{(m)}$$

Newton Kleinman method

low rank ADI method

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Step i: solve the projected linear system

$$(\mathcal{A} - \mathcal{B} \mathcal{K}^{(m)} + q_i \mathcal{M})^T \mathcal{V}_i = \mathcal{Y} \quad (1)$$

Newton Kleinman method

low rank ADI method

Krylov solver

Workflow

Nested Iteration

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Avoid explicit projection using [HEINKENSCHLOSS/SORENSEN/SUN '08]:

Newton Kleinman method

low rank ADI method

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Newton Kleinman method

low rank ADI method

Krylov solver

Avoid explicit projection using [HEINKENSCHLOSS/SORENSEN/SUN '08]:
Replace (1) and solve instead the saddle point system (SPS)

$$\begin{bmatrix} \mathcal{A}^T - (\mathcal{K}^{(m)})^T \mathcal{B}^T + q_i \mathcal{M}^T & \mathcal{G} \\ \mathcal{G}^T & 0 \end{bmatrix} \begin{bmatrix} \mathcal{V}_i \\ * \end{bmatrix} = \begin{bmatrix} \mathcal{Y} \\ 0 \end{bmatrix}$$

for different ADI shifts q_i for a couple of rhs \mathcal{Y} .



Workflow

Additional Tasks

- Compute initial feedback for unstable systems.
 - Determine the invariant unstable subspace \mathcal{U} .
 - Solve Bernoulli equation on \mathcal{U} [BENNER '11, AMODEI/BUCHOT '12].



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Workflow

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SPP1253

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SPP1253

OCIP 2012

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Workflow

Additional Tasks

SPP1253

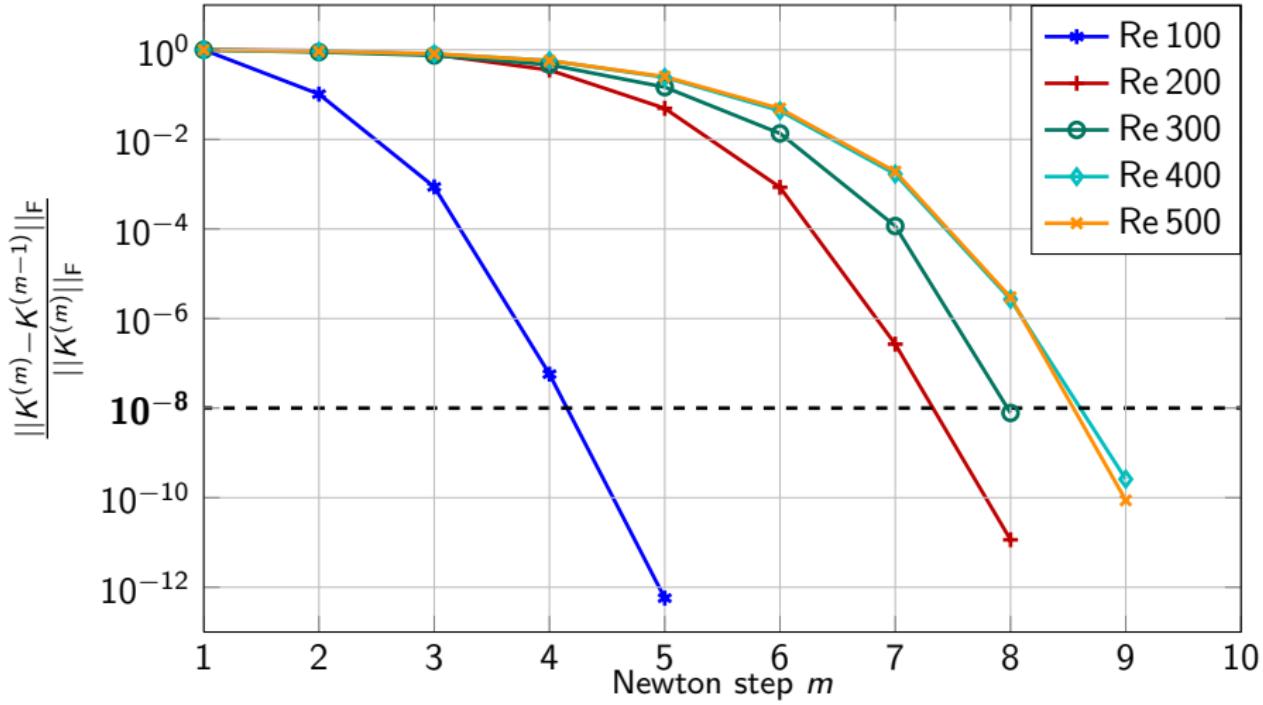
OCIP 2012

work in progress

- Compute initial feedback for unstable systems.
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Numerical Examples

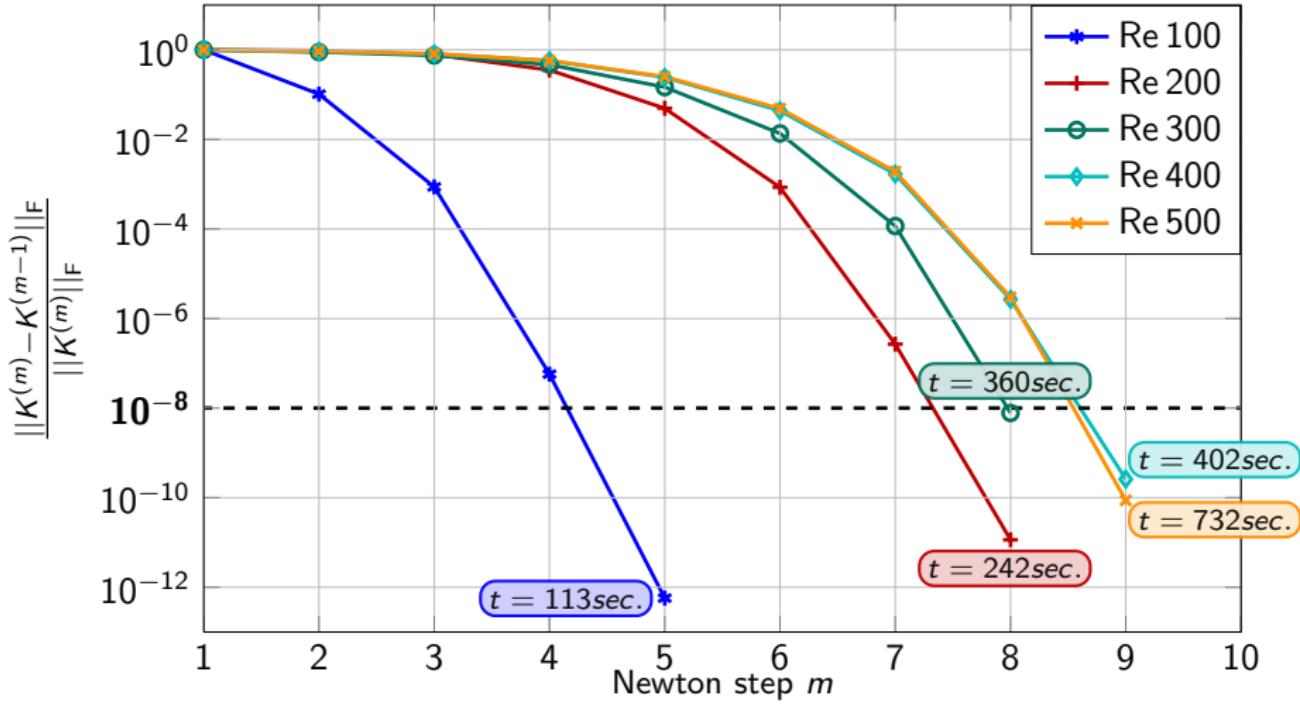
Newton-ADI: NSE on von Kármán Vortex Street



Relative change of feedback matrix K for different Reynolds numbers ($\lambda = \rho = 1$).

Numerical Examples

Newton-ADI: NSE on von Kármán Vortex Street

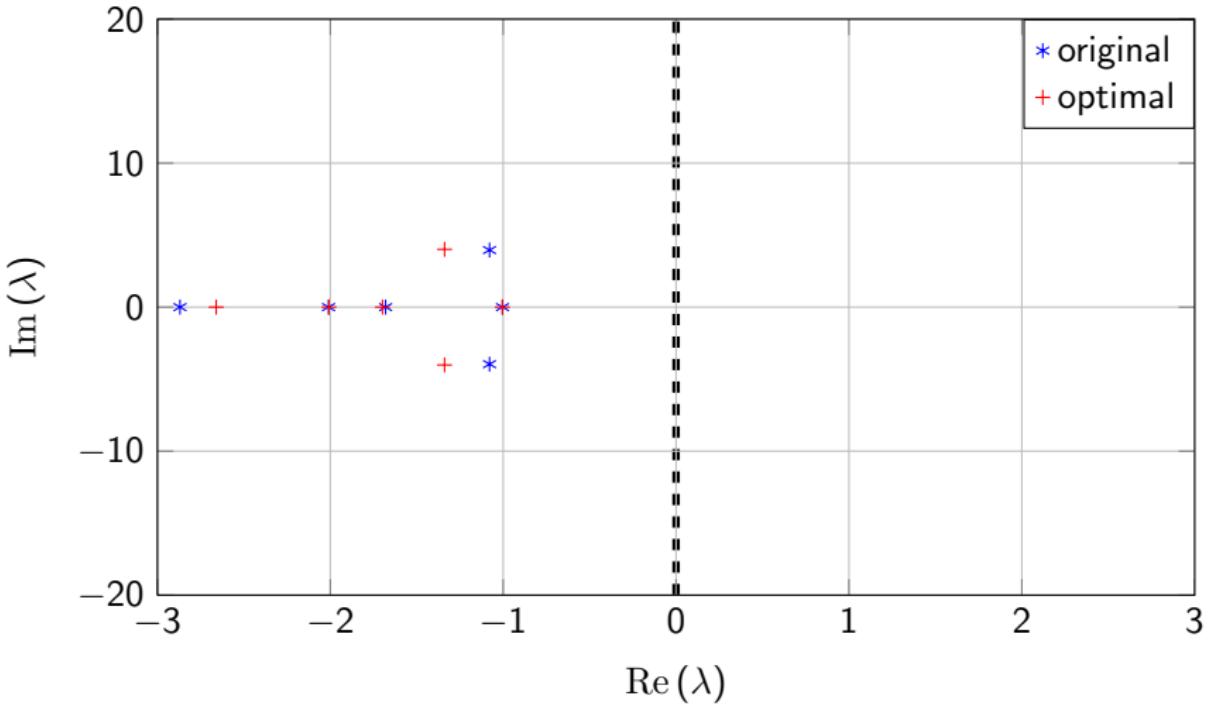


Relative change of feedback matrix K for different Reynolds numbers ($\lambda = \rho = 1$).

Numerical Examples

Eigenvalue Behavior of NSE on von Kármán Vortex Street

Zoom into eigenvalues for NSE pencil for: $\text{Re } 100$

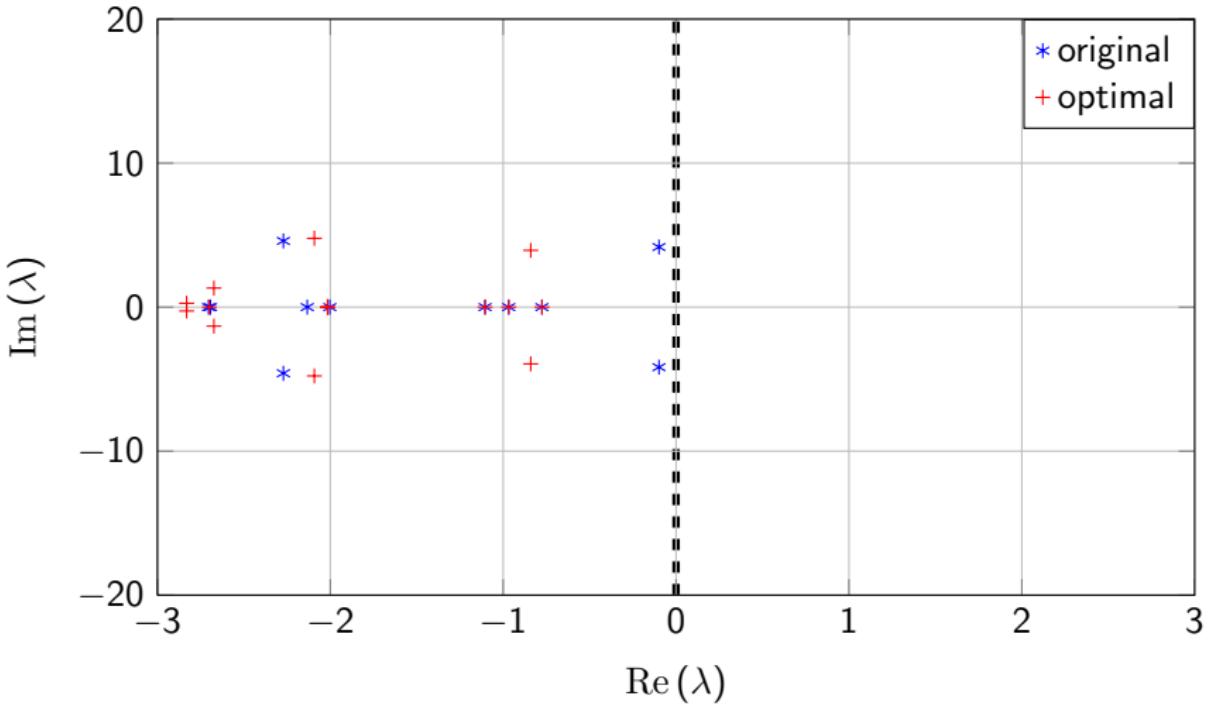


Numerical Examples

Eigenvalue Behavior of NSE on von Kármán Vortex Street



Zoom into eigenvalues for NSE pencil for: Re 200

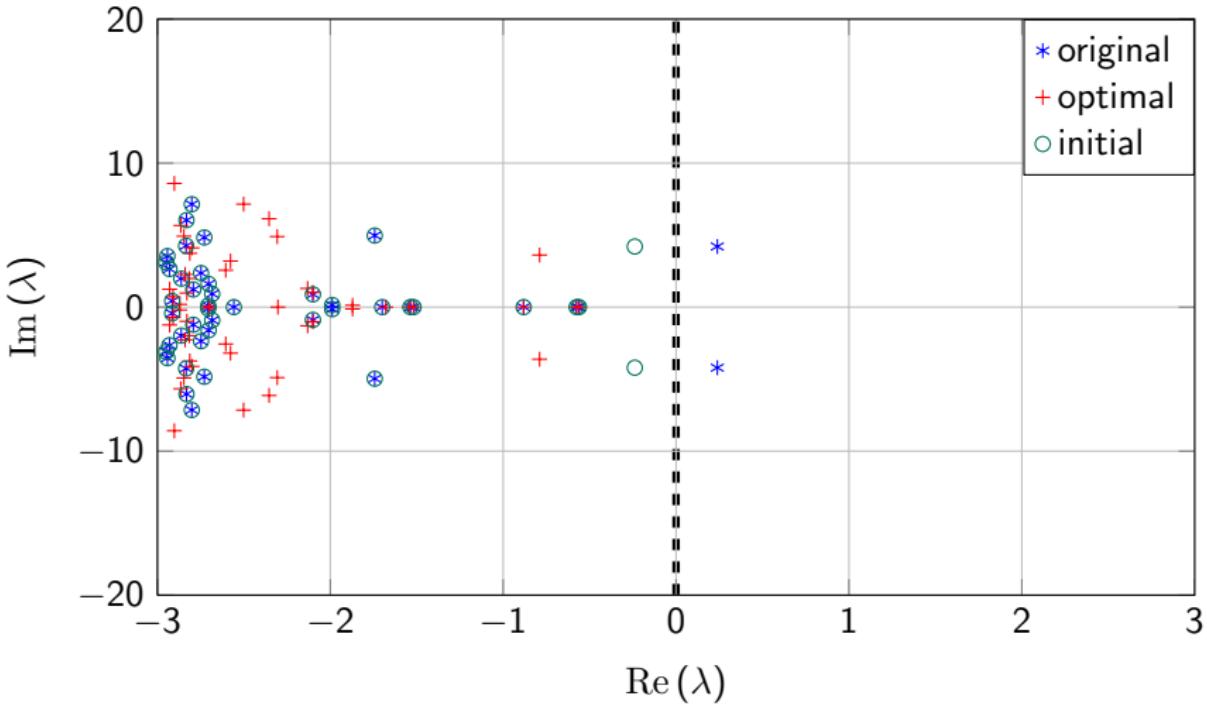


Numerical Examples

Eigenvalue Behavior of NSE on von Kármán Vortex Street



Zoom into eigenvalues for NSE pencil for: Re 300

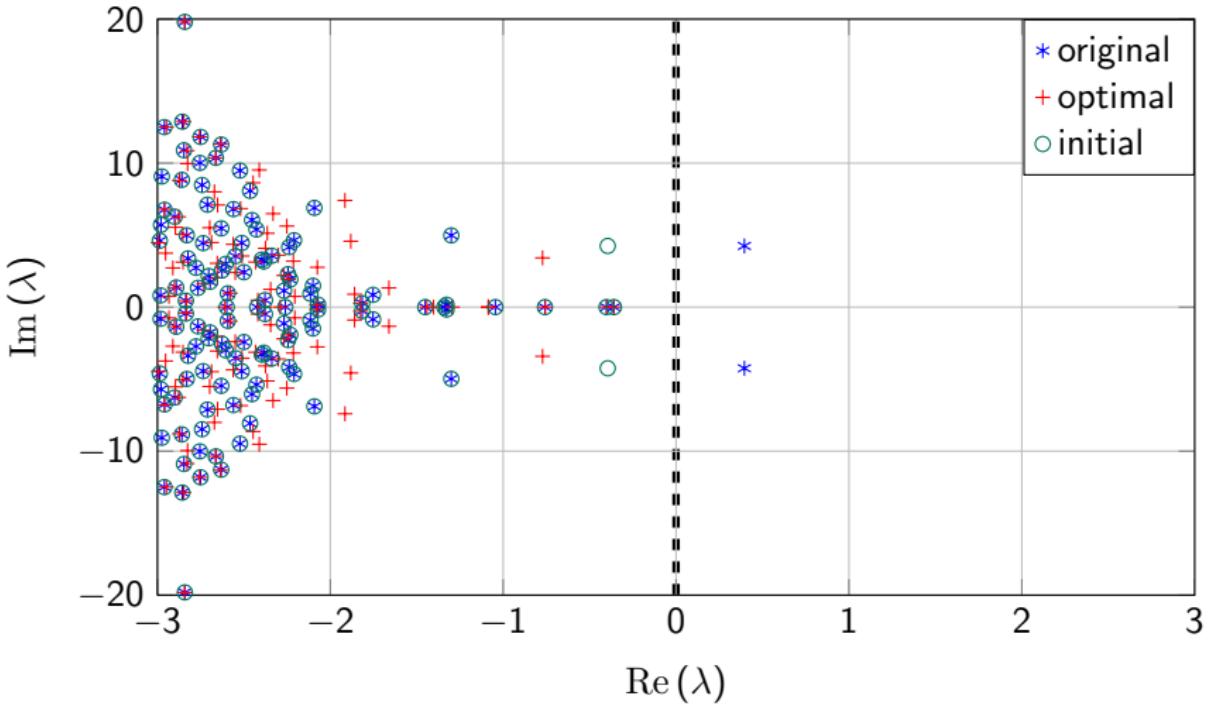


Numerical Examples

Eigenvalue Behavior of NSE on von Kármán Vortex Street



Zoom into eigenvalues for NSE pencil for: Re 400

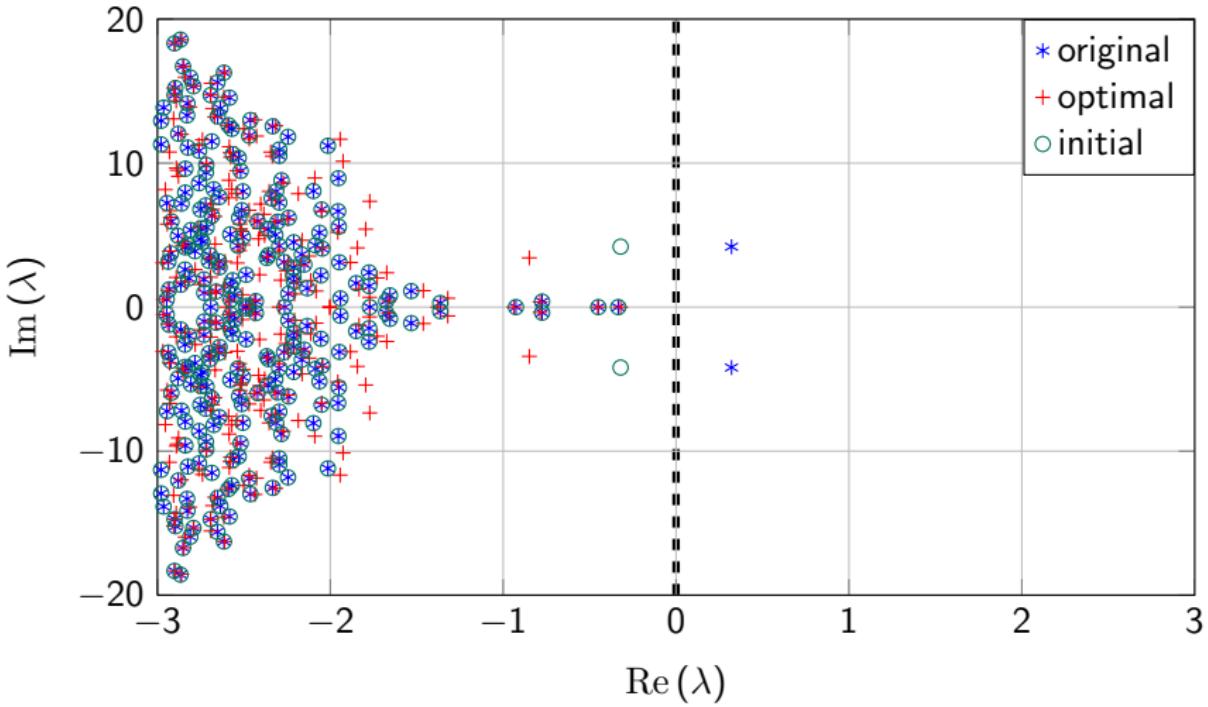


Numerical Examples

Eigenvalue Behavior of NSE on von Kármán Vortex Street



Zoom into eigenvalues for NSE pencil for: Re 500

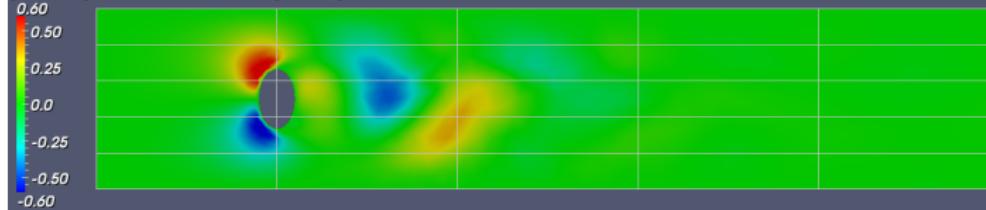


Numerical Examples

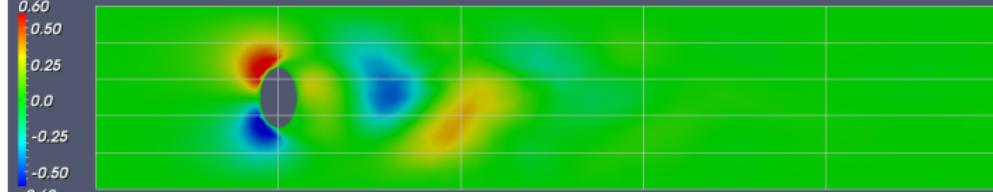
Closed-Loop Simulation of NSE on von Kármán Vortex Street for $Re = 300$



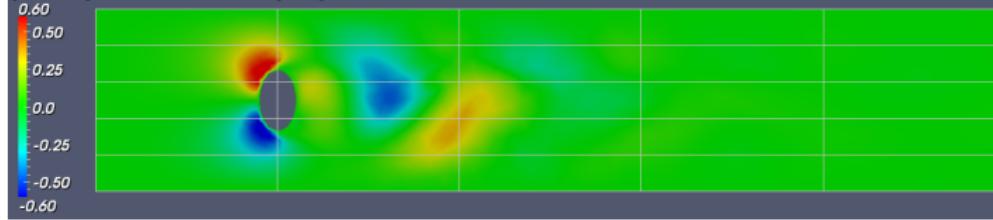
y-component of velocity (original flow)



y-component of velocity (initial feedback)



y-component of velocity (optimal feedback)





Numerical Examples

Closed-Loop Simulation of NSE on von Kármán Vortex Street for $Re = 300$



Conclusion

Review

- Adapt Newton-ADI algorithm and ADI shift determination for flow problems (DAE structure).
- Improved input matrix B w.r.t. Raymond's analytic approach.
- Closed-loop simulation for NSE.
- Adapted method to coupled flow in reactor model.
- Developed suitable output matrix C for reactor model.

Outlook

- Improve idea of *inexact Newton* to threefold nested iteration.
- Residual based stopping criteria for feedback computation.
- Closed-loop simulation of coupled flow in reactor model.
- Improve Krylov solver via the use of recycling or block techniques.
- Non-conforming finite elements that guarantee $\operatorname{div} \vec{v} = 0$.

↪ MPI Preprint: [BENNER/SAAK/SCHIEWECK/SKRZYPACZ/W. '12]

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Literature



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