

Non-Conforming Finite Elements and Riccati-Based Feedback Stabilization of the Stokes Equations

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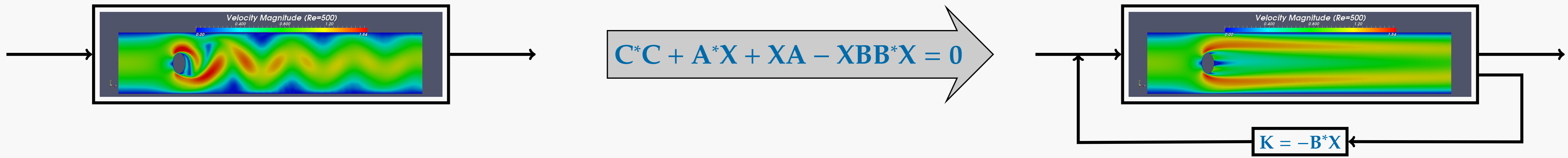
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Goal



Problem Setting

Abstract Problem Setting

Motivation:

- Stabilization of flows described by Navier-Stokes equations (NSE)

$$\left. \begin{aligned} \frac{\partial}{\partial t} \mathbf{v} - \frac{1}{\text{Re}} \Delta \mathbf{v} + \mathbf{v} \cdot \nabla \mathbf{v} + \nabla p = \mathbf{0} \\ \text{div } \mathbf{v} = 0 \end{aligned} \right\} \text{in } (0, \infty) \times \Omega, \quad (1)$$

to steady-state solution, with $\Omega \subset \mathbb{R}^d, d = 2, 3$, the velocity field $\mathbf{v}(t, \mathbf{x}) \in \mathbb{R}^d$, the pressure $p(t, \mathbf{x}) \in \mathbb{R}$, the time $t \in (0, \infty)$, the spatial variable $\mathbf{x} \in \Omega$, and the Reynolds number $\text{Re} \in \mathbb{R}^+$.

- Construction based on associated linear quadratic control problem (LQR) for boundary control [4].
- Numerical treatment for 2D case with linearized NSE described in [1].

Here: Stokes equations

$$\left. \begin{aligned} \frac{\partial}{\partial t} \mathbf{v} - \frac{1}{\text{Re}} \Delta \mathbf{v} + \nabla p = \mathbf{0} \\ \text{div } \mathbf{v} = 0 \end{aligned} \right\} \text{in } (0, \infty) \times \Omega. \quad (2)$$

Semi Discretized Problem Setting

Finite element discretization of (2) yields

$$\begin{aligned} M \dot{\mathbf{z}} &= A \mathbf{z} + G \mathbf{p} + B \mathbf{u}, \\ \mathbf{0} &= G^T \mathbf{z}, \\ \mathbf{y} &= C \mathbf{z}, \end{aligned} \quad (3)$$

with

- discretized velocity $\mathbf{z}(t) \in \mathbb{R}^{n_v}$ and pressure $\mathbf{p}(t) \in \mathbb{R}^{n_p}$,
- symmetric positive definite mass matrix $M \in \mathbb{R}^{n_v \times n_v}$,
- system matrix $A \in \mathbb{R}^{n_v \times n_v}$ (symmetric for Stokes) and
- discretized gradient $G \in \mathbb{R}^{n_v \times n_p}$ of rank n_p .

In the context of an LQR problem one additionally gets

- the input matrix $B \in \mathbb{R}^{n_v \times n_r}$ and
- the input $\mathbf{u}(t) \in \mathbb{R}^{n_r}$,

which describe the boundary control. Partial observation furthermore leads to

- the output $\mathbf{y}(t) \in \mathbb{R}^{n_o}$ and
- the output matrix $C \in \mathbb{R}^{n_o \times n_v}$.

Implicit Index Reduction

To rewrite the DAE system (3) with differential index two as a generalized state space system, we use the projector

$$\Pi^T = I - M^{-T} G (G^T M^{-1} G)^T,$$

defined in [3]. The projected ODE system is of the form

$$\begin{aligned} M \dot{\mathbf{z}} &= \mathcal{A} \mathbf{z} + \mathcal{B} \mathbf{u}, \\ \mathbf{y} &= C \mathbf{z}, \end{aligned} \quad (4)$$

with $M = M^T > 0$ and $\mathbf{z}(t) \in \mathbb{R}^{n_v - n_p}$.

To solve the algebraic Riccati equation associated to the system (4) we use a Newton-ADI-method. Instead of solving the projected dense Lyapunov equations in the innermost loop, we use [3, Lemma 5.2] and have to solve the saddle point system

$$\begin{bmatrix} A^T + \mu_i M^T & G \\ G^T & 0 \end{bmatrix} \begin{bmatrix} \Lambda \\ * \end{bmatrix} = \begin{bmatrix} Y \\ 0 \end{bmatrix}, \quad (5)$$

for a couple of right hand sides Y and a different shift μ_i in each ADI step during each Newton step.

Contribution Details

Following [3] equation (4) is the semi discretized formulation of (2) including boundary data and projected to the manifold of divergence free discrete functions.

The pair $(\mathcal{A}, \mathcal{E})$ then implements the semi discretized, projected spatial differential operator from (2).

For $i = 1$ and $X_0 = 0$ for every column in V_j equation (6), (or (5) respectively) corresponds to solving a modified stationary Stokes problem:

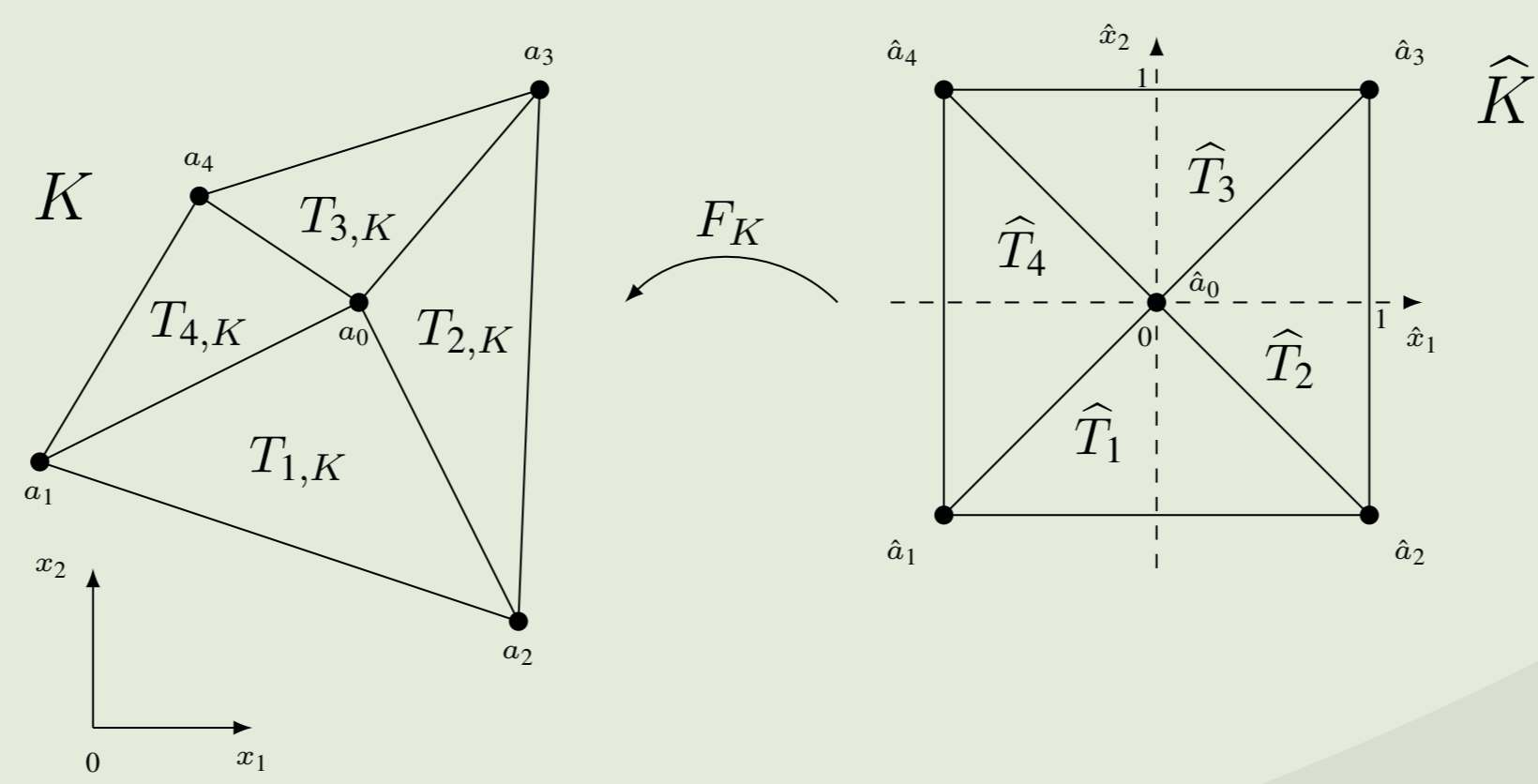
$$\begin{aligned} -\frac{1}{\text{Re}} (\nabla \mathbf{v}_{j,k} \cdot \nabla \varphi) + (p, \text{div } \varphi) + \mu_j (\mathbf{v}_{j,k}, \varphi) &= (\mathbf{v}_{j-1,k}, \varphi), \\ (\text{div } \mathbf{v}, \psi) &= 0, \end{aligned} \quad (7)$$

for test functions $\varphi \in (H^1(\Omega))^2$ – respecting the boundary conditions – and $\psi \in L^2(\Omega)$, in the evaluation of the k -th column of (6)/(5).

Similarly applications of \mathcal{A} and M can be pulled back to the weak formulation level.

Advantages:

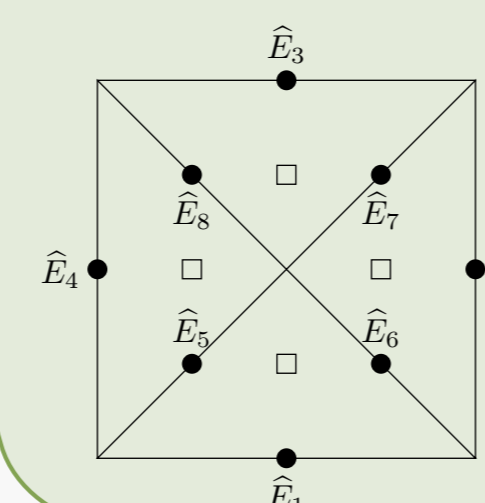
- (7) allows higher flexibility of formulation (e.g., adapting [5]),
- possibility to work matrix free,
- parallel implementations can exploit full FEM, PDE or domain features.



The composite cell $K = F_K(\hat{K})$, where $F_{K|T_i} \in [P_1(\hat{T}_i)]^2$.

Features of the composite non-conforming element [2]:

- inf-sup stable,
- low computational costs,
- pointwise mass-conservation within the son-triangles,
- L_2 orthogonal basis for velocity \Rightarrow diagonal mass matrix,
- after static condensation of interior dofs only $2 \times 4 + 1$ dofs per cell \Rightarrow produce a better stencil compared to the conforming case,
- optimal approximation order on general meshes,
- easy implementation.



Numbering of the edges of the son-triangles on the reference element and local degrees of freedom (dofs) of the composite $P_1^{\text{nc}}(\hat{K})$ -element (marked by \bullet for velocity and \square for pressure dofs)

Newton Kleinman Method Approximate X solving:

$$C^T C + \mathcal{A}^T X M + M^T X \mathcal{A} - M^T X B B^T X M = 0$$

In step i solve the Lyapunov equation:

$$(\mathcal{A}^T - K_{i-1}^T B^T) X_i M + M^T X_i (\mathcal{A} - B K_{i-1}) = -G_{i-1} G_{i-1}^T,$$

where $K_{i-1} = B^T X_{i-1} M$ and $G_{i-1} = [C^T, K_{i-1}]$.

Applying the low rank ADI algorithm requires to solve

$$(\mathcal{A}_i + \mu_j M)^T V_j = M V_{j-1}, \quad (6)$$

with $\mathcal{A}_i = \mathcal{A}^T - K_{i-1}^T B^T$ for a possibly complex μ_j in each step.

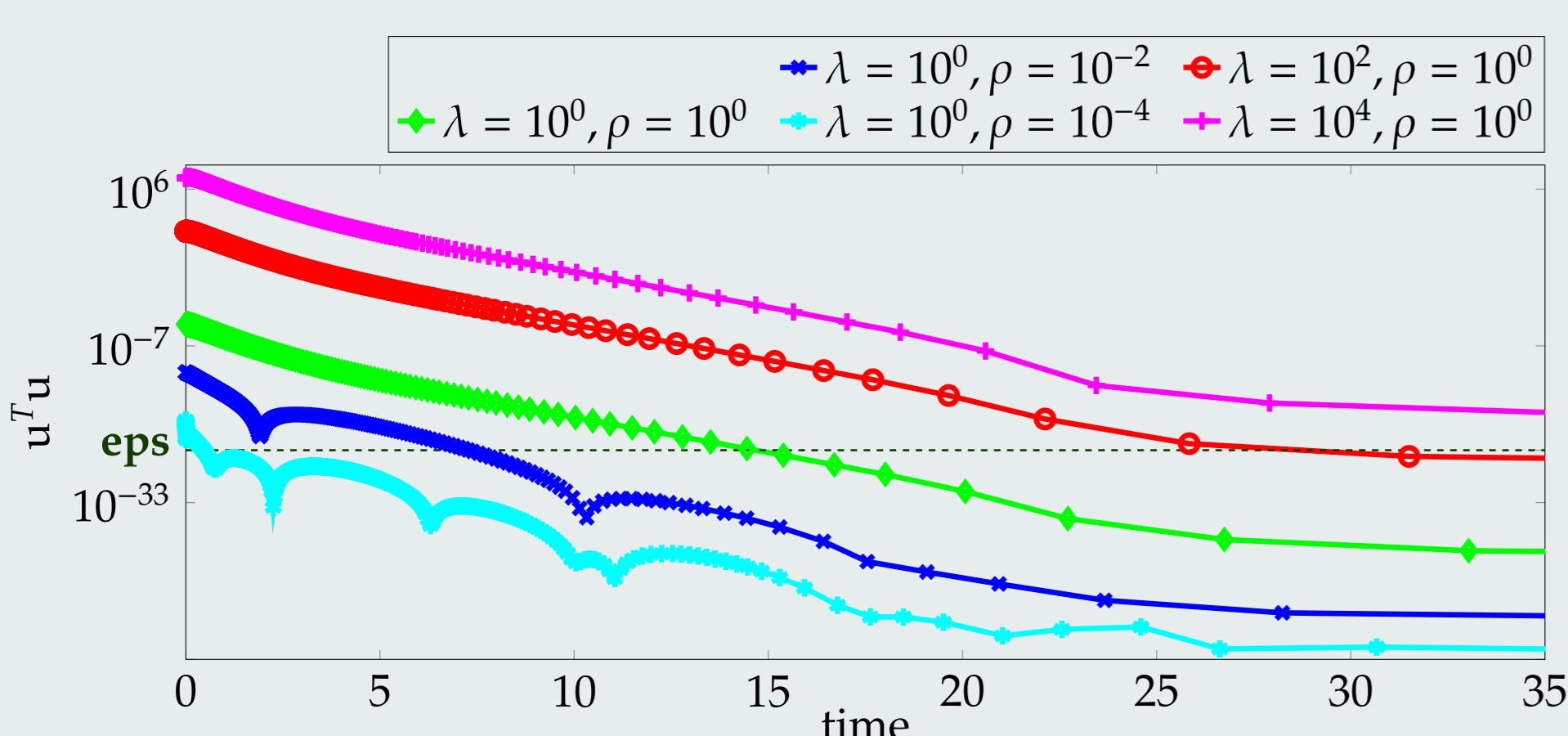
Solve (5) instead of (6) to increase efficiency. Requires:

- Sherman-Morrison-Woodbury formula,
- block preconditioning (e.g., [2]),
- investigation of required accuracies, i.e., inexact Newton-Kleinman-ADI.

New here:

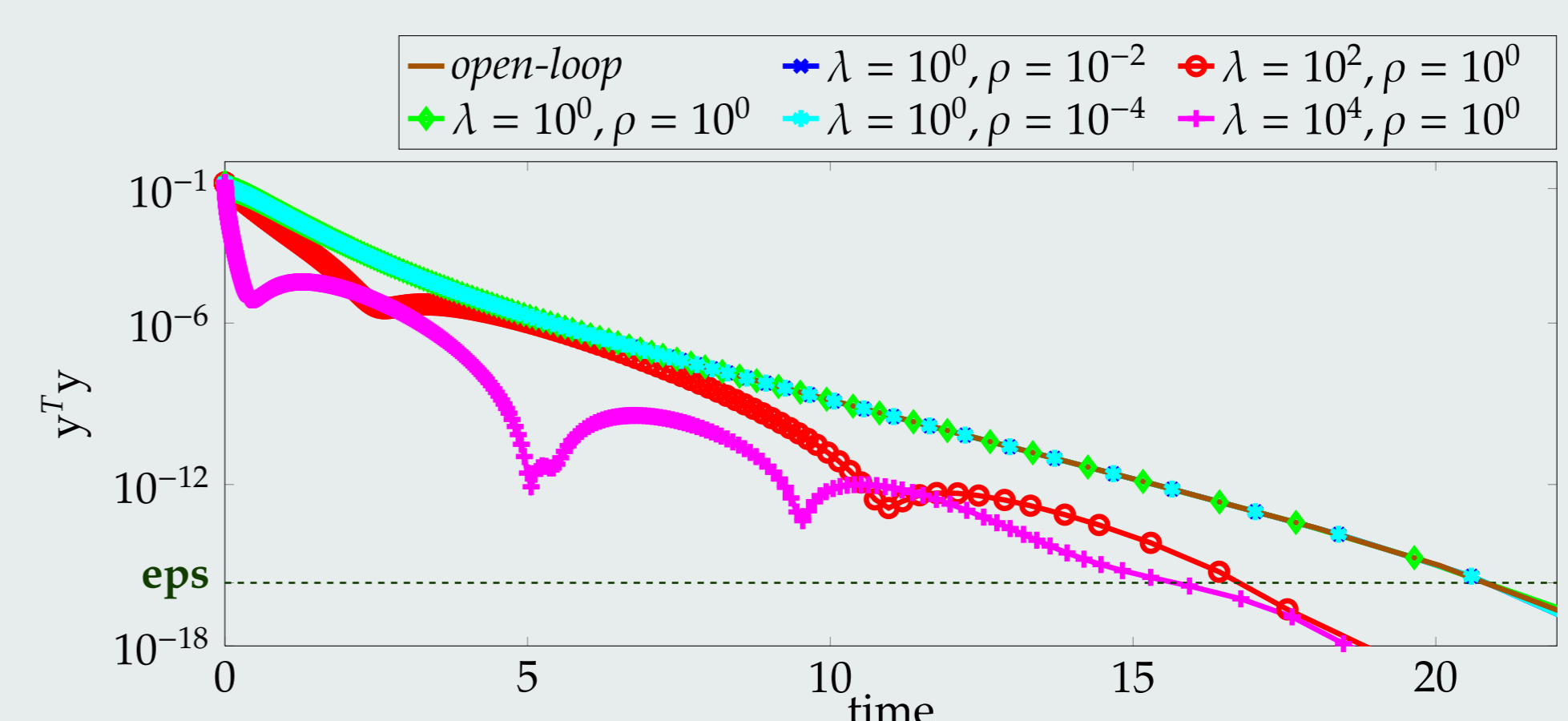
- Investigation of special finite elements that help ensuring “divergence free”-condition. for inexact solves.
- Interpretation of (5) in terms of the original PDE system.

Numerical Results



Evolution of control and output \Rightarrow for the cost function

$$\mathcal{J}(y, u) = \frac{1}{2} \int_0^\infty \lambda \|y\|^2 + \frac{1}{\rho} \|u\|^2 dt.$$



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